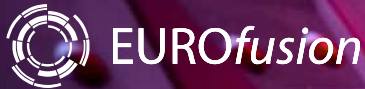
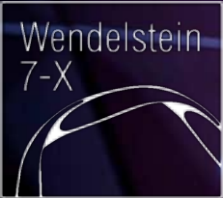




# Introduction to multi-channel spectrometers



O. P. Ford



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# Introduction

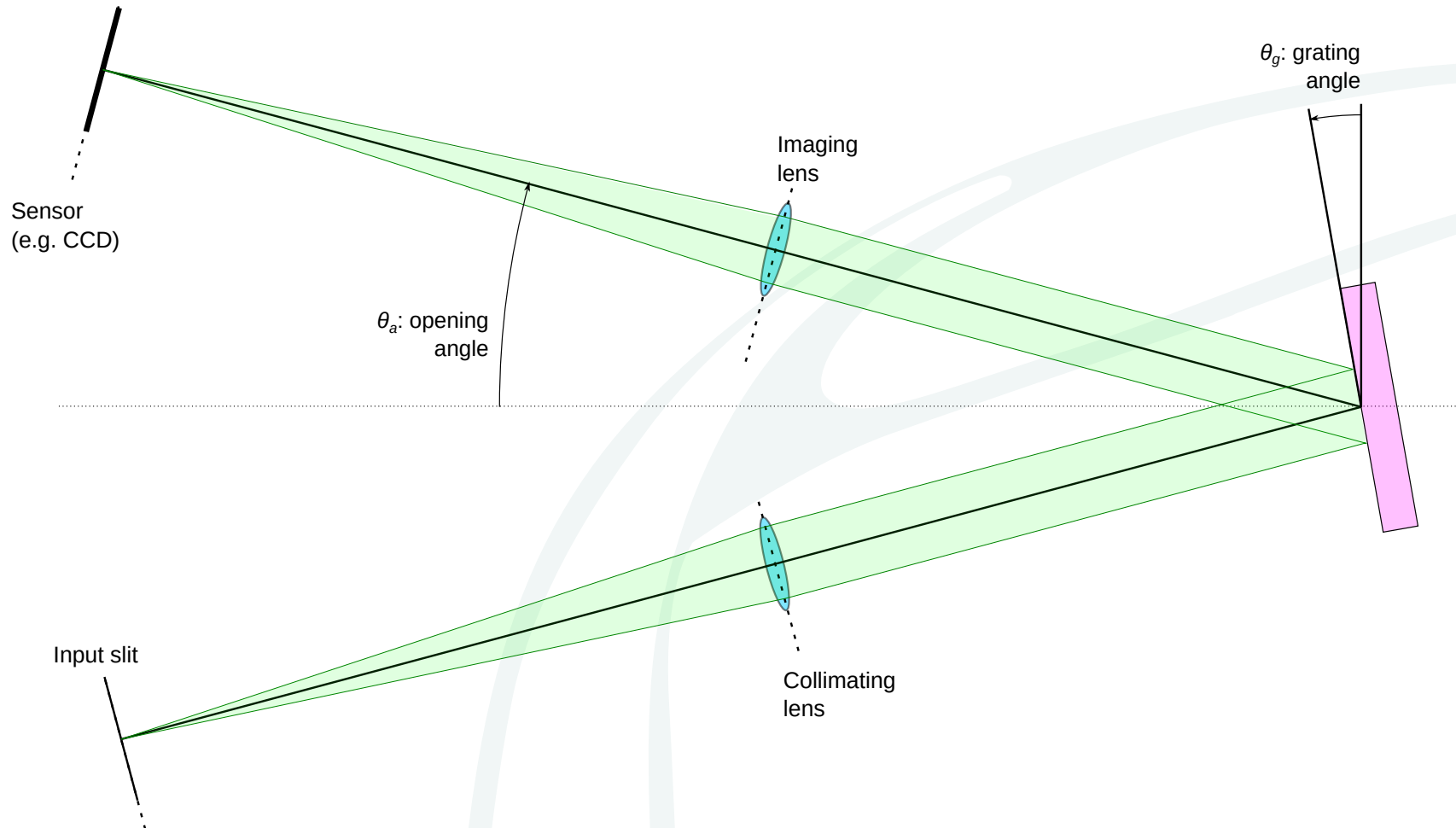


Short introduction to multi-channel spectrometers:

- Basic principles
- Configuration and design
- Set-up
- Alignment
- Calibration

# Principle

Simple spectrometers usually based on a slit and a diffraction grating.  
Usually fixed input and output arms with rotating reflection grating.



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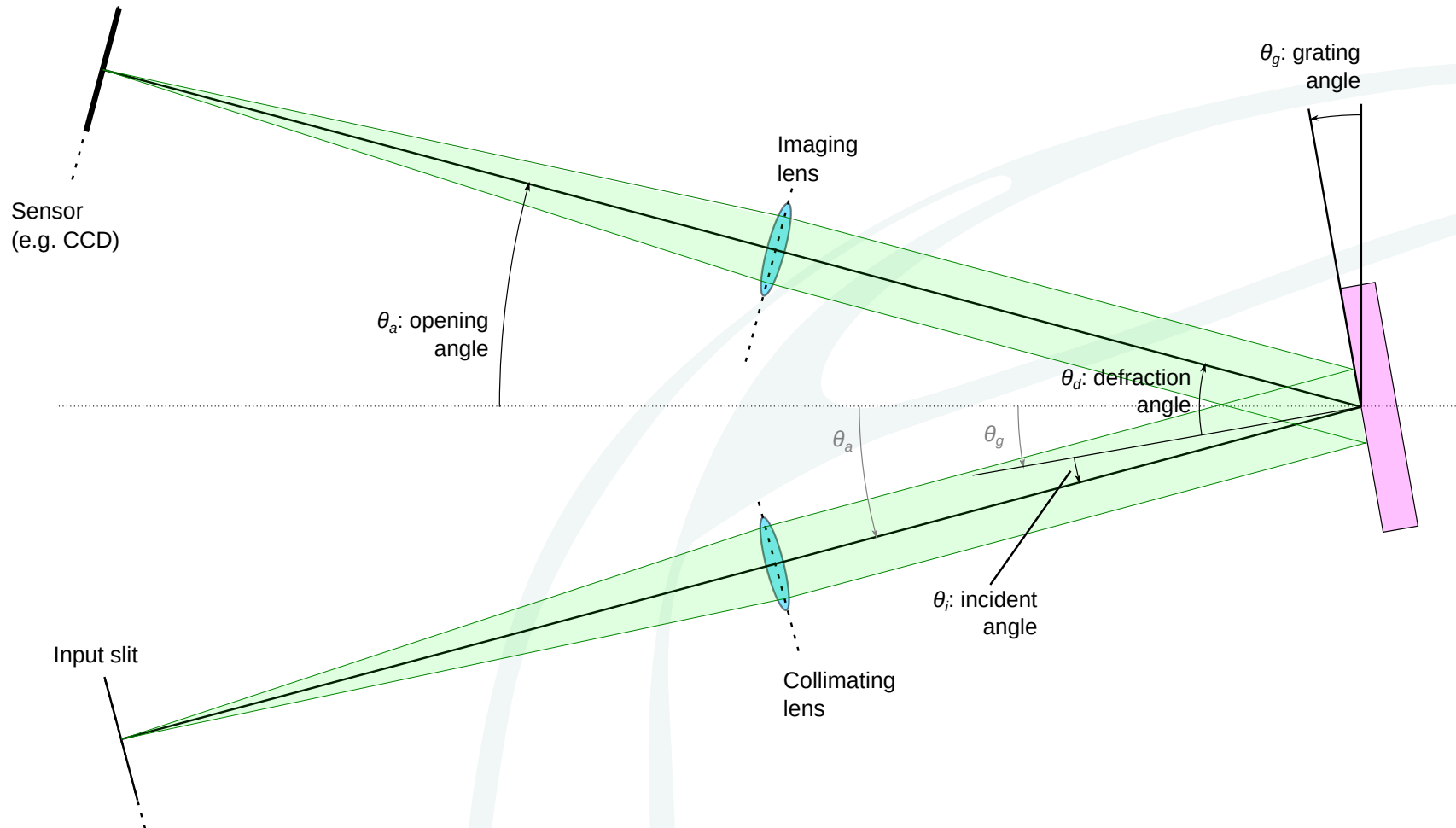
Incidence and diffraction angles:

$$\begin{aligned}\theta_d &= \theta_a + \theta_g & \theta_a &= (\theta_d + \theta_i)/2 \\ \theta_i &= \theta_a - \theta_g & \theta_g &= (\theta_d - \theta_i)/2\end{aligned}$$

Diffraction equation:

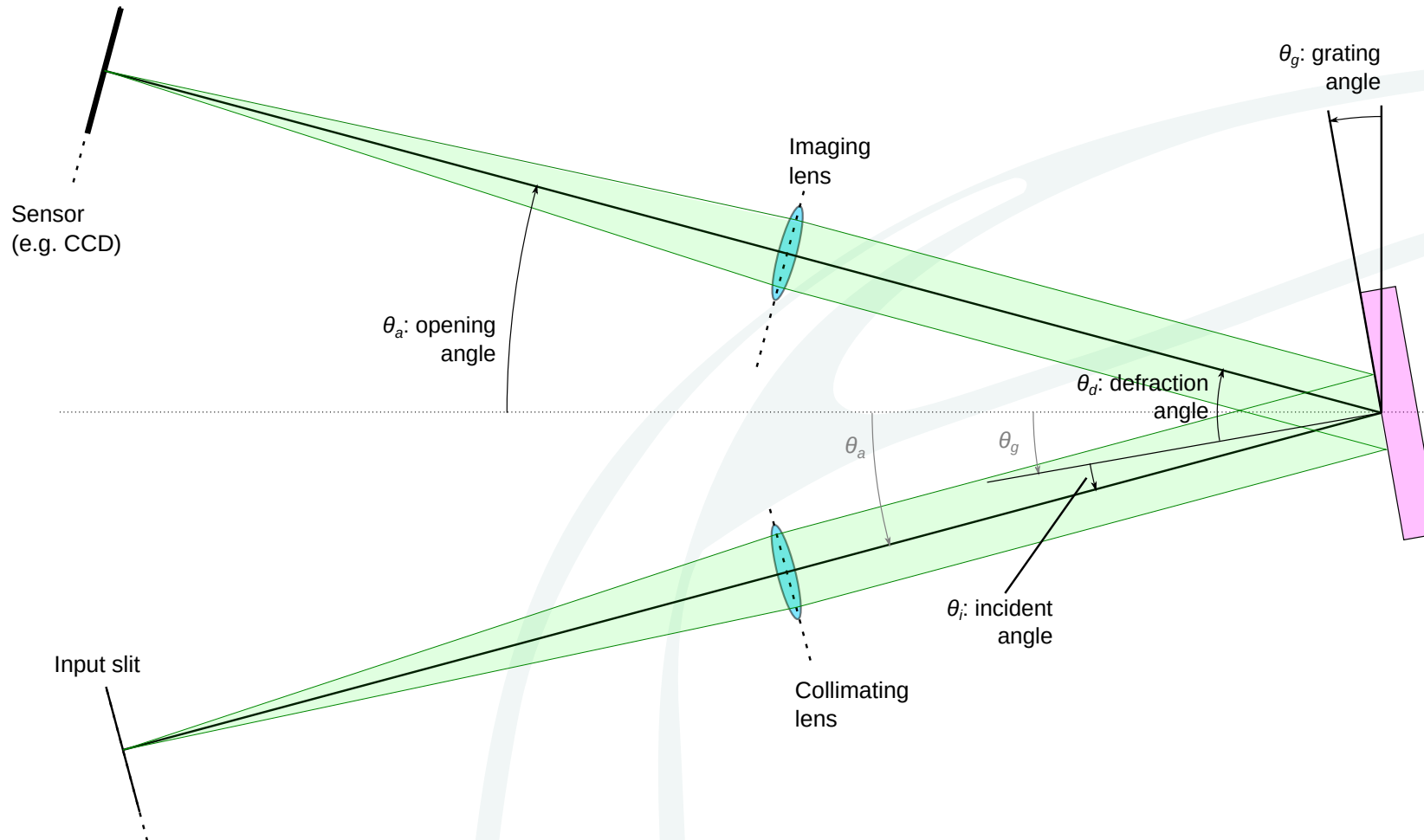
$$\sin \theta_d - \sin \theta_i = k n \lambda$$

$k$  = diffraction order  
(use +1 or -1, otherwise a filter is required to select the order)  
 $n$  = grating grooves [ $\text{m}^{-1}$ ]  
 $\lambda$  = wavelength [m]



# Principle

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Usually fixed input and output arms with rotating reflection grating.



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$$\theta_d = \theta_a + \theta_g \quad \theta_a = (\theta_d + \theta_i)/2$$
$$\theta_i = \theta_a - \theta_g \quad \theta_g = (\theta_d - \theta_i)/2$$

Diffraction equation:

$$\sin \theta_d - \sin \theta_i = k n \lambda$$

- $k$  = diffraction order  
(use +1 or -1, otherwise a filter is required to select the order)
- $n$  = grating grooves [ $\text{m}^{-1}$ ]
- $\lambda$  = wavelength [m]

Central wavelength:

$$\sin(\theta_a + \theta_g) - \sin(\theta_a - \theta_g) = k n \lambda$$
$$\lambda = 2 \cos \theta_a \sin \theta_g / k n$$

Setting of grating for given wavelength:

$$\sin \theta_g = k n \lambda / (2 \cos \theta_a)$$

# Wavelength range

Simple spectrometers usually based on a slit and a diffraction grating.  
Usually fixed input and output arms with rotating reflection grating.

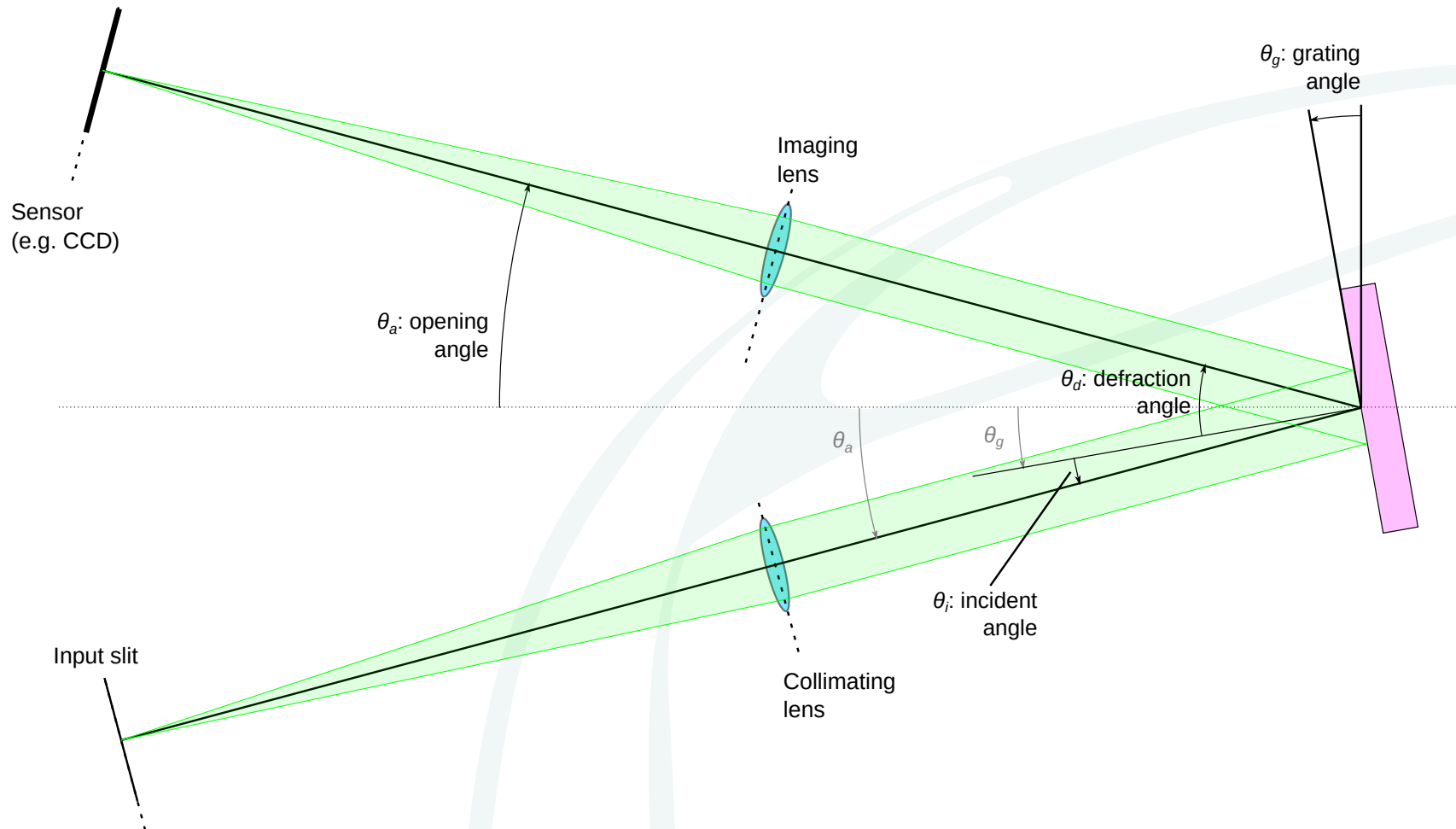
$$\theta_d = \theta_a + \theta_g \quad \theta_a = (\theta_d + \theta_i)/2$$

$$\theta_i = \theta_a - \theta_g \quad \theta_g = (\theta_d - \theta_i)/2$$

$$\sin \theta_d - \sin \theta_i = k n \lambda$$

Dispersion:

$$d\lambda/d\theta_d = \cos(\theta_a + \theta_g) / k n$$



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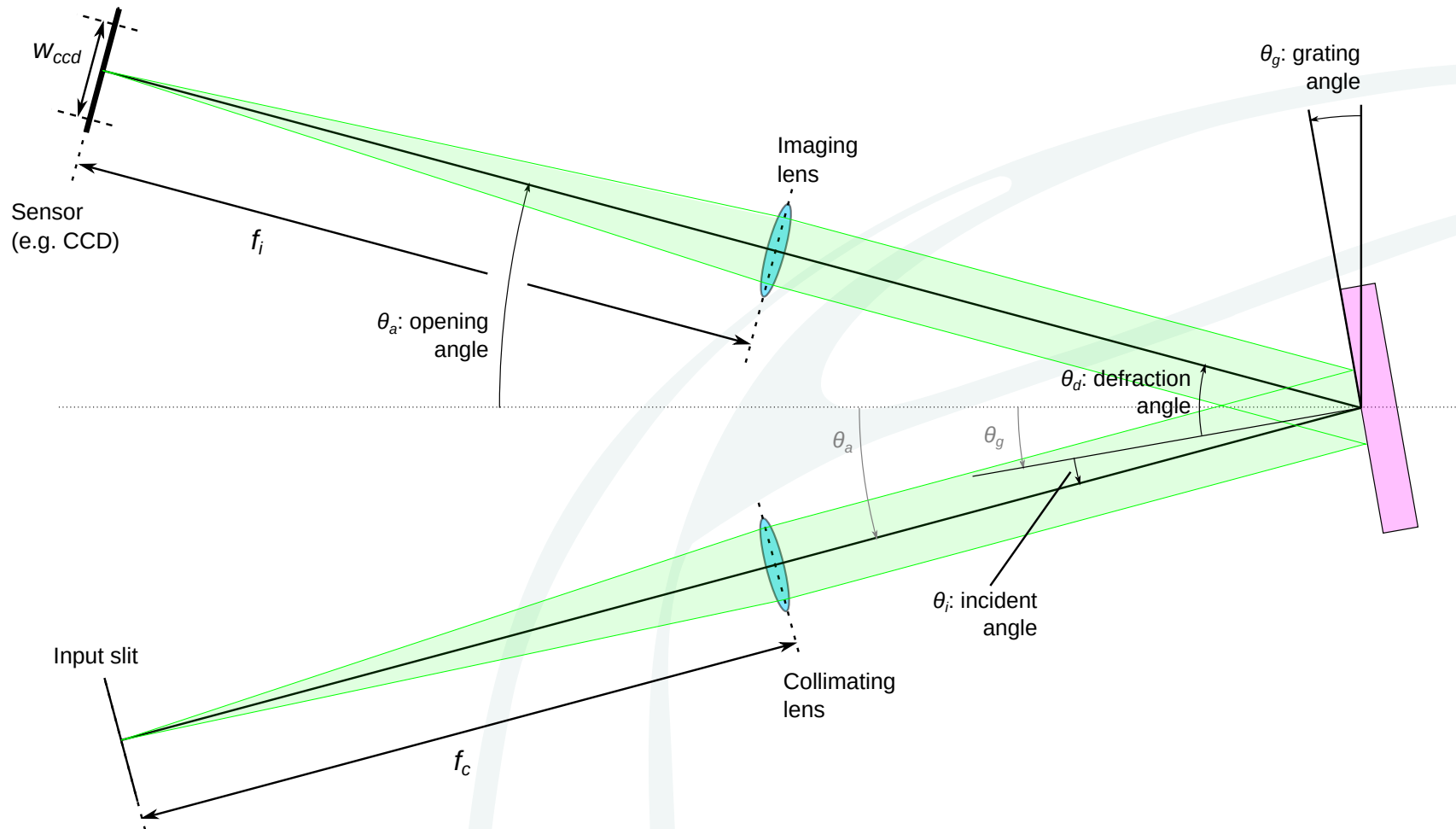
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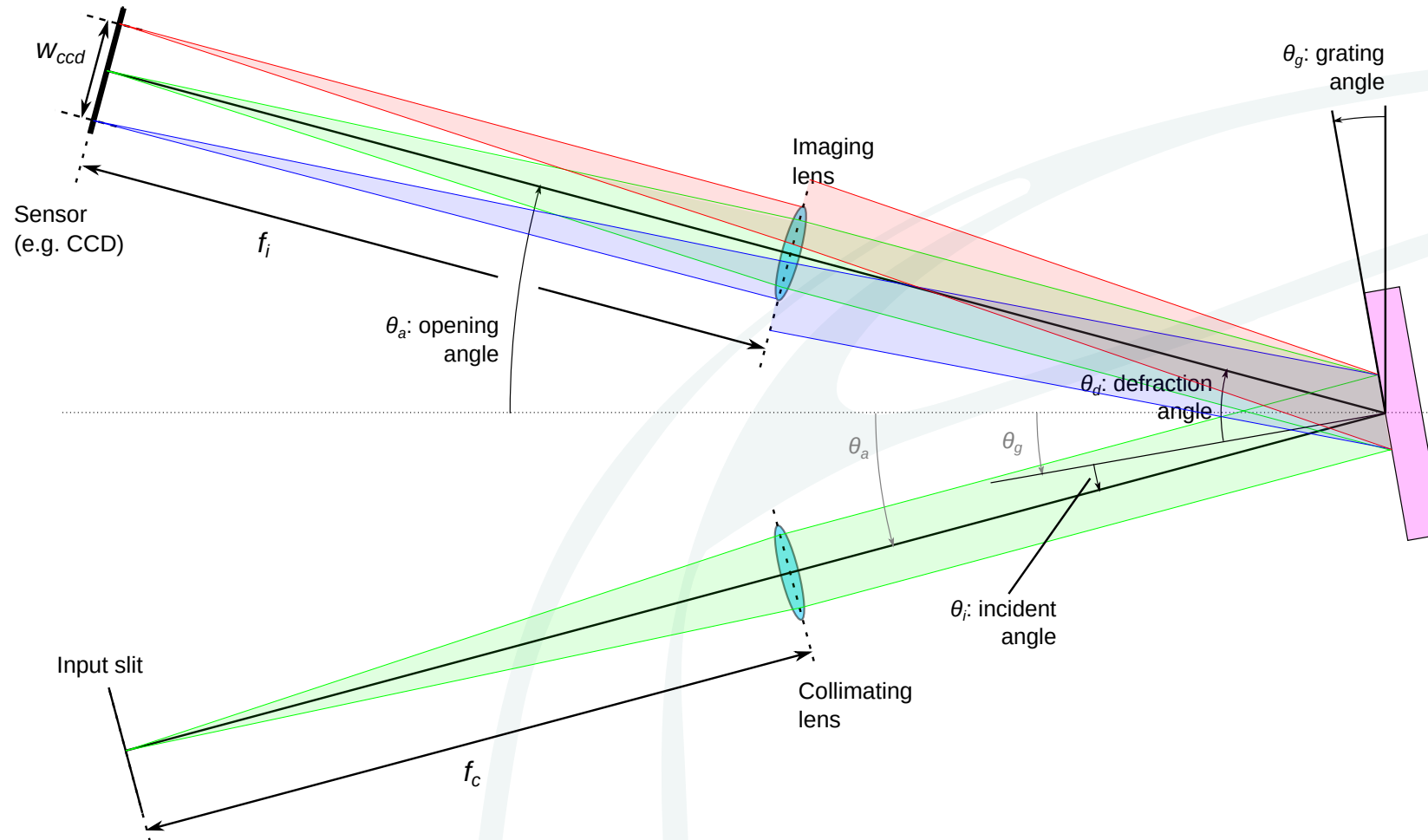
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Dispersion:

$$d\lambda/d\theta_d = \cos(\theta_a + \theta_g) / k n$$

Wavelength range on sensor:

$$\Delta\lambda = d\lambda/d\theta_d \cdot w_{ccd} / f_i$$

$$= w_{ccd} / f_i \cos(\theta_a + \theta_g) / k n$$

$$= w_{ccd} / f_i [ (1 - \frac{1}{4}k^2n^2\lambda^2)^{1/2} / kn - \theta_a \frac{1}{2} \lambda - \theta_a^2 / (kn (4 - k^2n^2\lambda^2)^{1/2}) ]$$

--> Weird function of  $\theta_a$  and  $\lambda$ :

- larger  $\theta_a$
  - larger  $\lambda$
  - larger  $n$
  - larger  $k$
- } higher resolution / less wavelength range



# Wavelength range

Wavelength range on sensor:

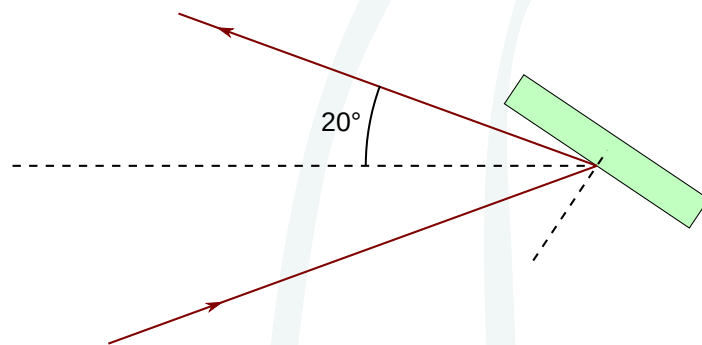
$$\Delta\lambda = \lambda w_s/f_i [ \text{sqrt}( 4 \cos^2 \theta_a /k^2n^2\lambda^2 - 1) - \tan \theta_a ] / 2$$

Example: AUG1/2 with PI ProEM 1024x:  
(CXRS narrow range for single line)

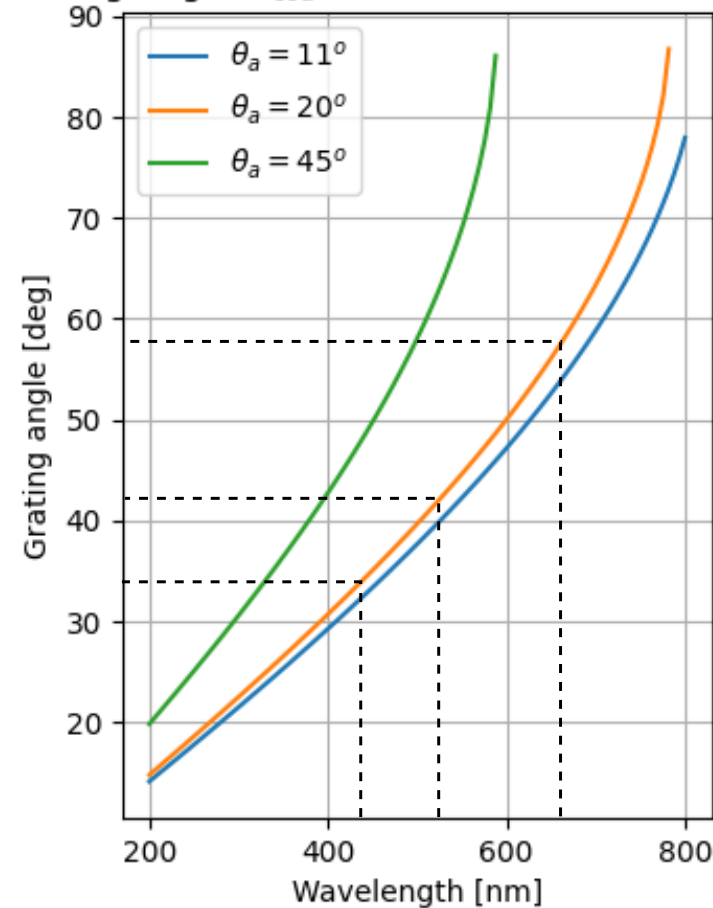
$k = 1$   
 $n = 2400 \text{ mm}^{-1}$   
 $\theta_a = 20^\circ$   
 $w_{ccd} = 1024 \times 13\mu\text{m} = 13.3\text{mm}$   
 $f_i = 200\text{mm}$

$\lambda$ [nm]	$\theta_g$ [°]	$\Delta\lambda$ [nm]
430	33.3	16.5
530	42.6	12.8
650	56.1	6.7

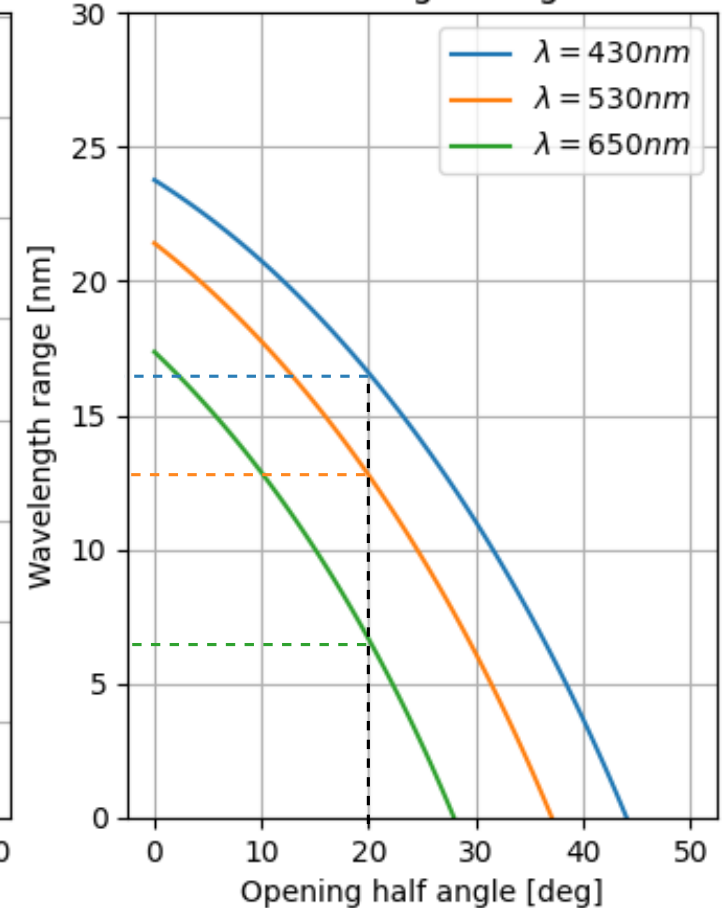
( $\theta_i$  is -ve!)



Grating angle  $w_{ccd} = 13\text{mm}$ ,  $n=2400\text{mm}^{-1}$ ,  $k=1$



Wavelength range



# Wavelength range

Wavelength range on sensor:

$$\Delta\lambda = \lambda w_s / f_i [ \text{sqrt}( 4 \cos^2 \theta_a / k^2 n^2 \lambda^2 - 1 ) - \tan \theta_a ] / 2$$

Example 2: SpexM500 with PCO Edge

for wide overview spectrum:

$$k = 1$$

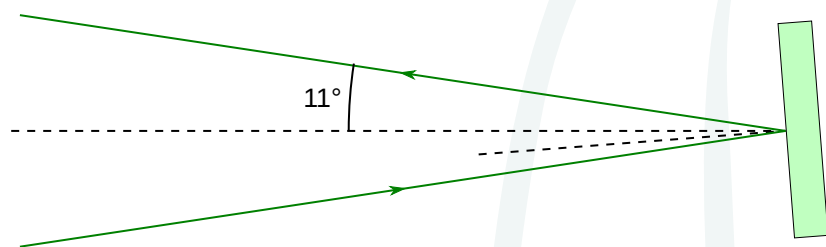
$$n = 300 \text{ mm}^{-1}$$

$$\theta_a = 10^\circ$$

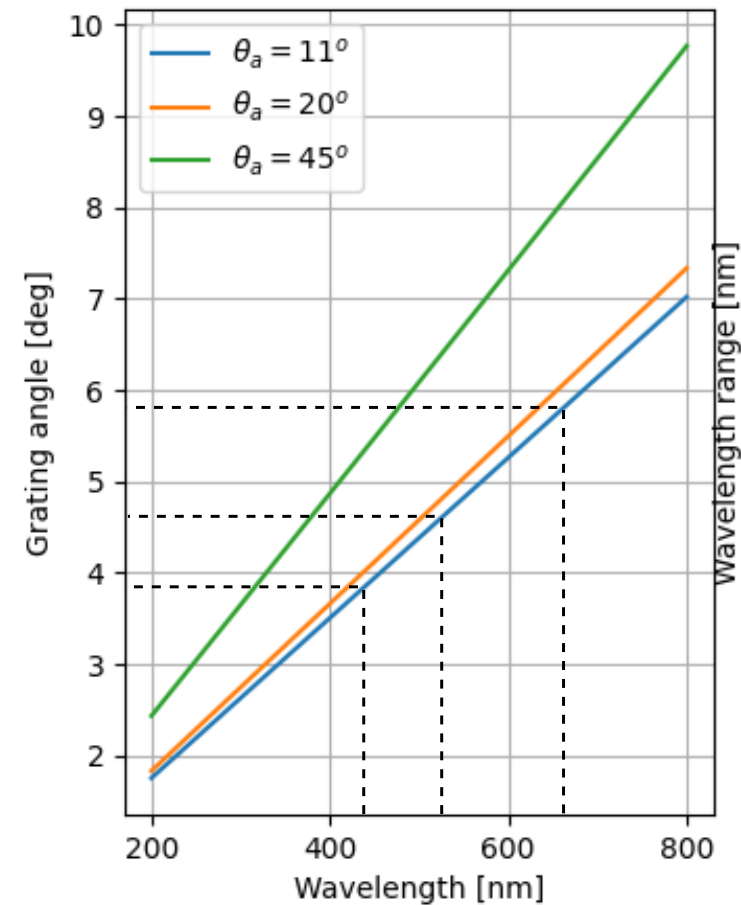
$$w_{\text{ccd}} = 2560 \times 6.5 \mu\text{m} = 16.6 \text{ mm}$$

$$f_i = 500 \text{ mm}$$

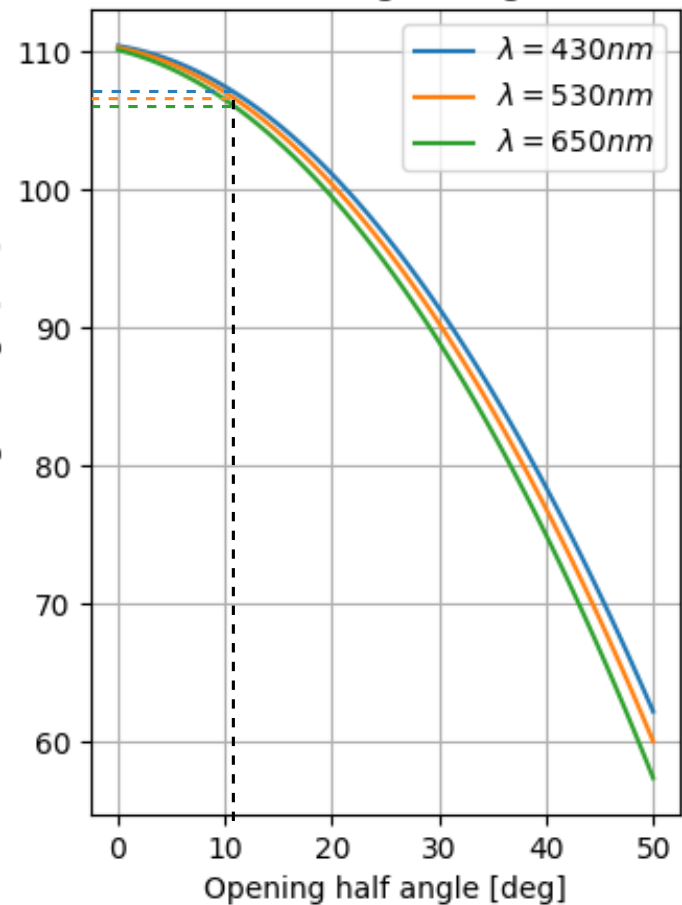
$\lambda$ [nm]	$\theta_g$ [°]	$\Delta\lambda$ [nm]
430	3.9	107
530	4.6	107
650	5.8	106



Grating angle  $w_{\text{ccd}} = 17 \text{ mm}$ ,  $n = 300 \text{ mm}^{-1}$ ,  $k = 1$

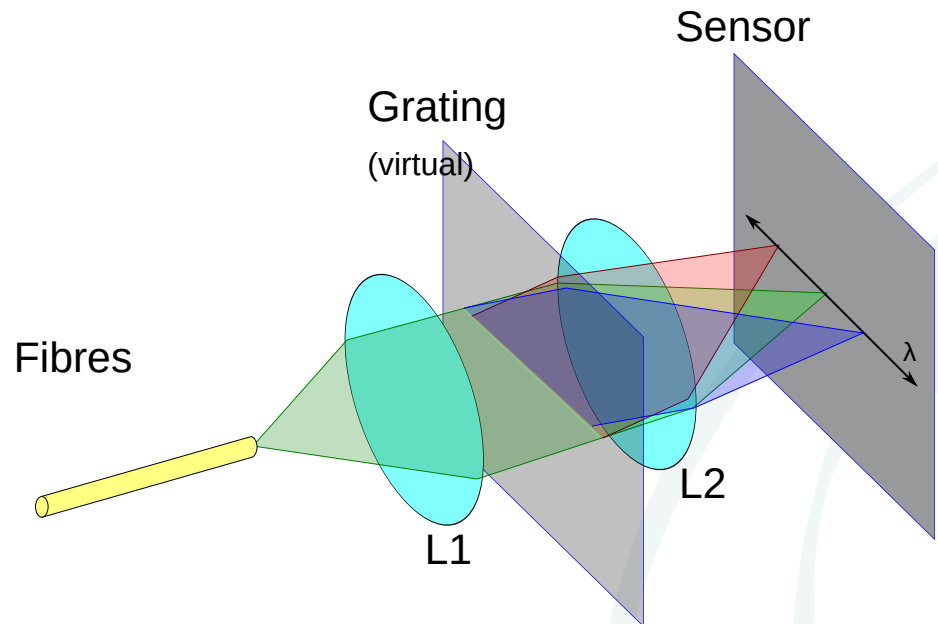


Wavelength range



# Multi-channel vertical

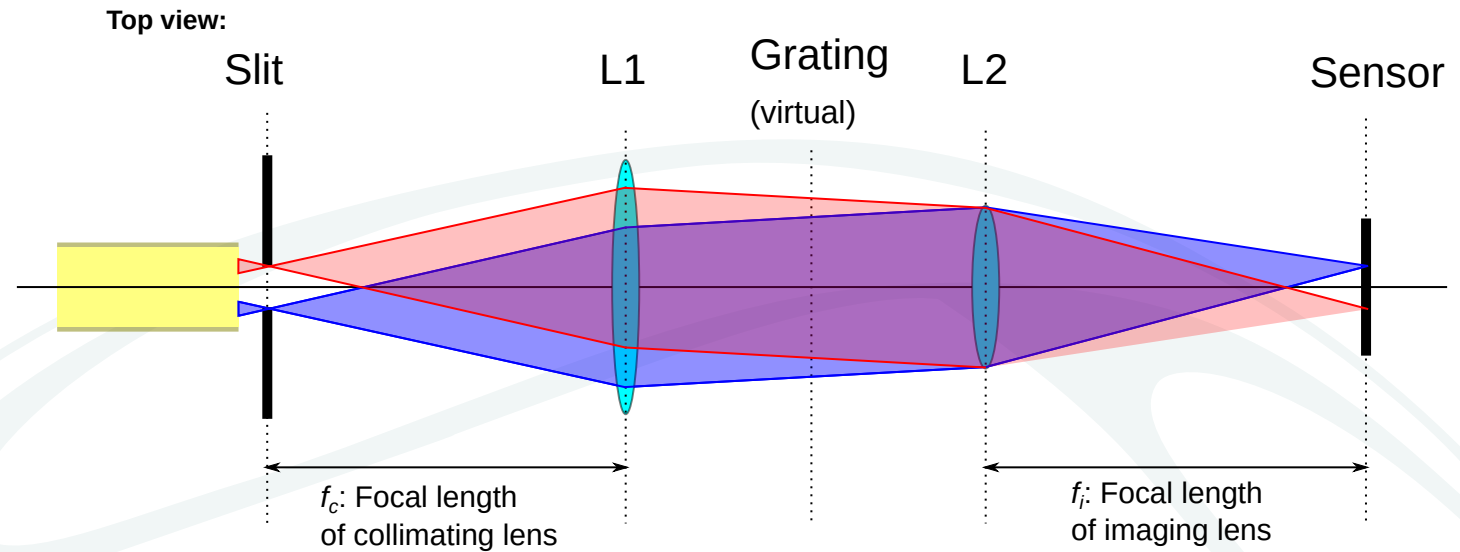
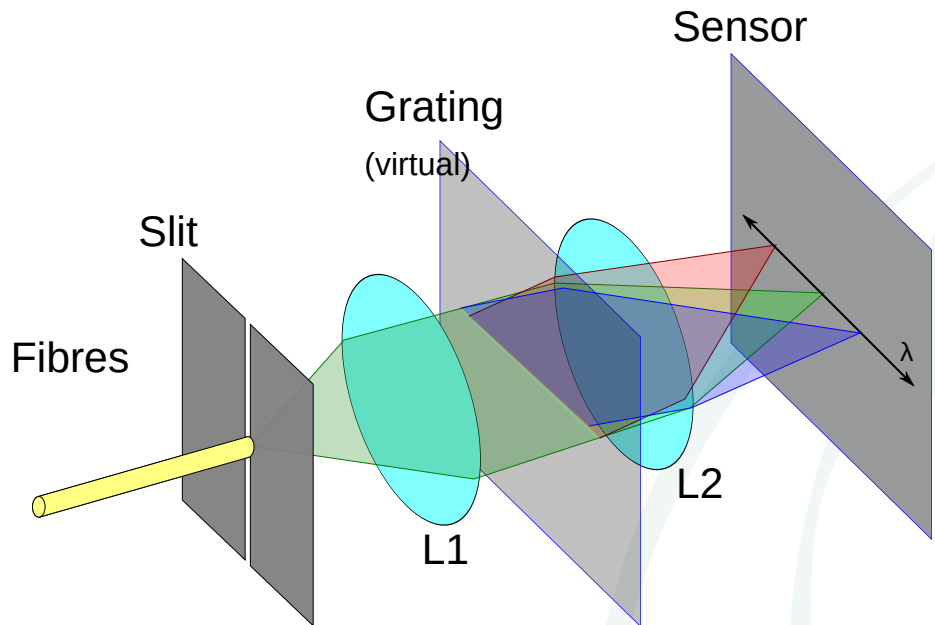
Simple multi-channel: Diffraction direction in horizontal plane.



# Multi-channel vertical

Simple multi-channel: Diffraction direction in horizontal plane.

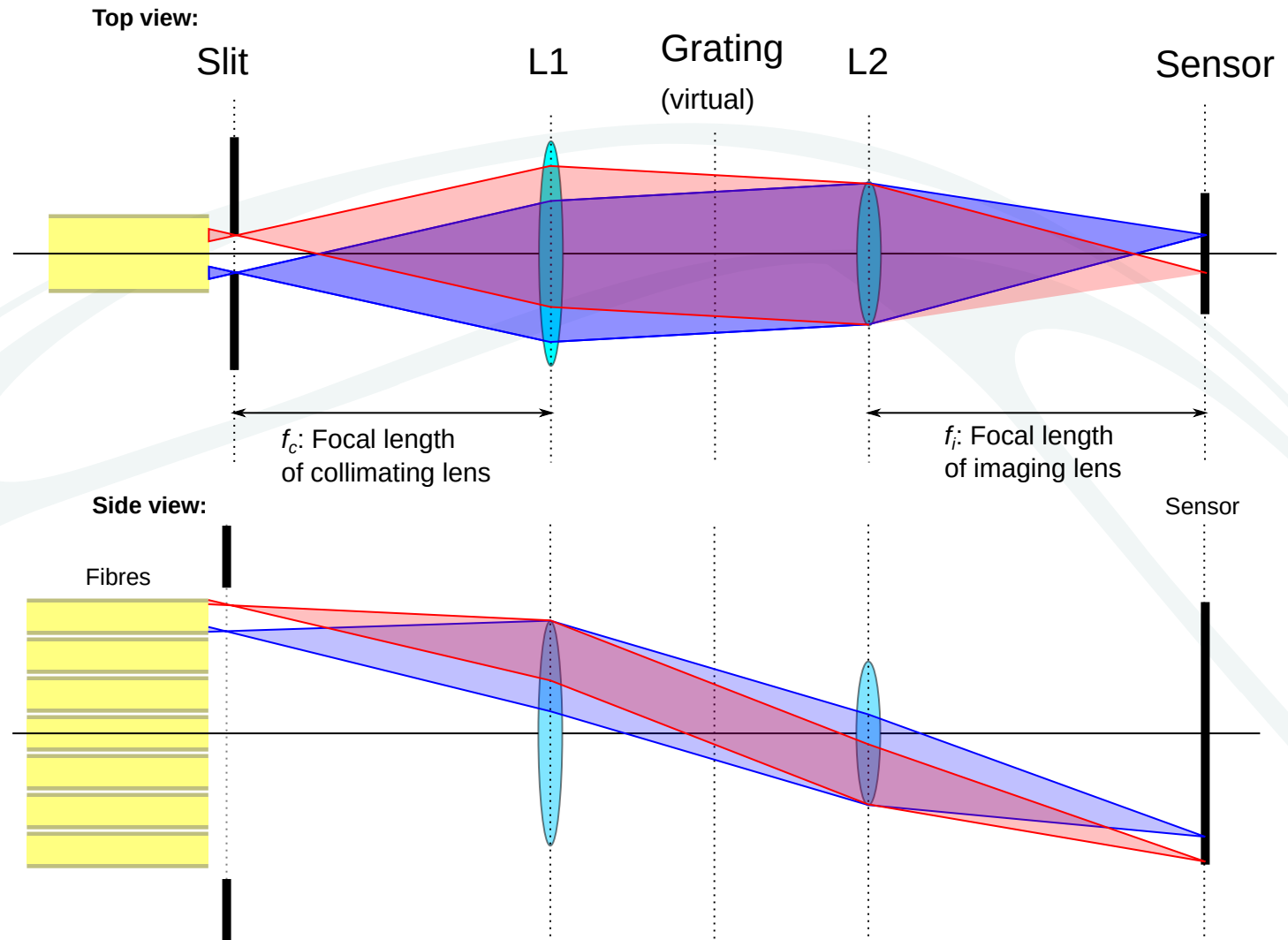
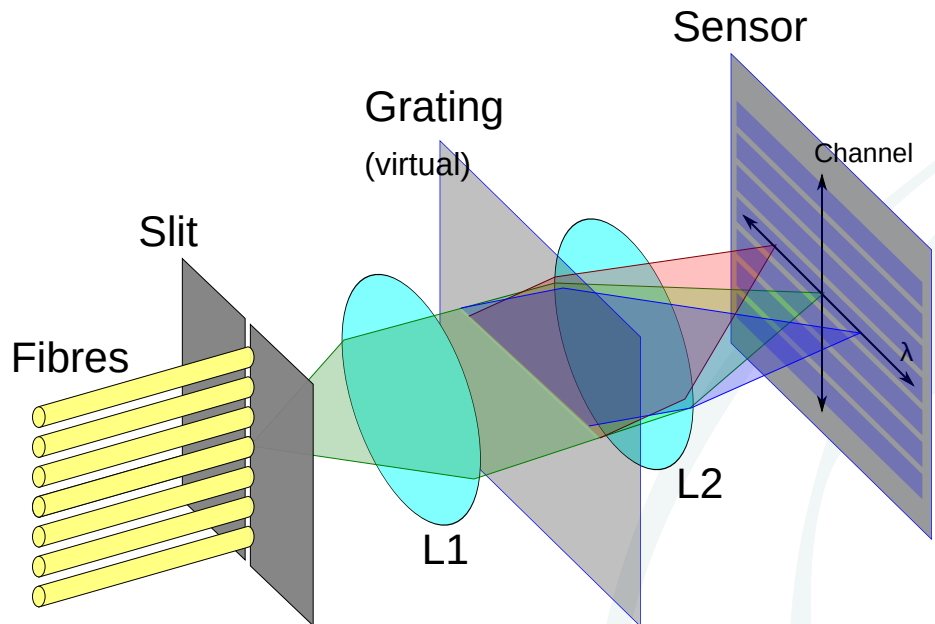
- Slit placed in front of input fibres to limit width.
- Slit imaged onto sensor in horizontal plane.



# Multi-channel vertical

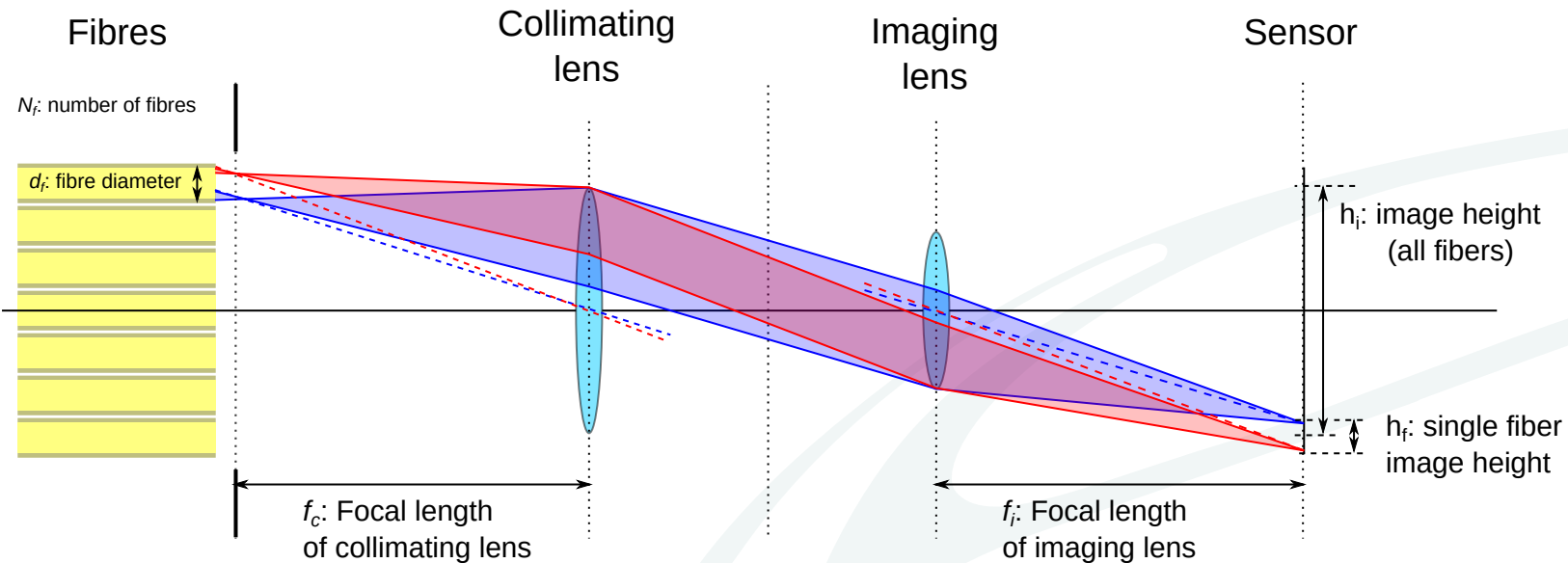
Simple multi-channel: Diffraction direction in horizontal plane.

- Slit placed in front of input fibres to limit width.
- Slit imaged onto sensor in horizontal plane.
- Multiple fibres imaged onto sensor in vertical plane.



# Magnification

Magnification is set by ratio of imaging and collimating lens.



Magnification:  $M = f_i / f_c$

Image height:  $h_i = M * (N_f * d_f)$

Fibre image size:  $h_f = M * d_f$

--> **Number of fibers limited by sensor height and ratio of focal lengths.**

$$N_f = h_i f_c / (f_i * d_f)$$

# Resolution

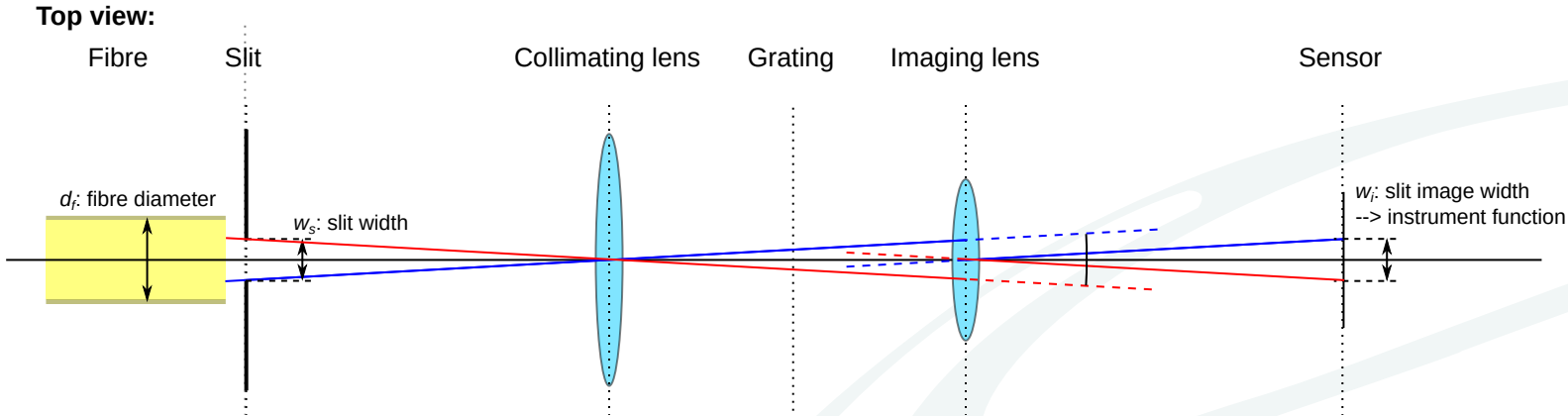


Magnification and slit width determine wavelength resolution:



# Resolution

Magnification and slit width determine wavelength resolution:



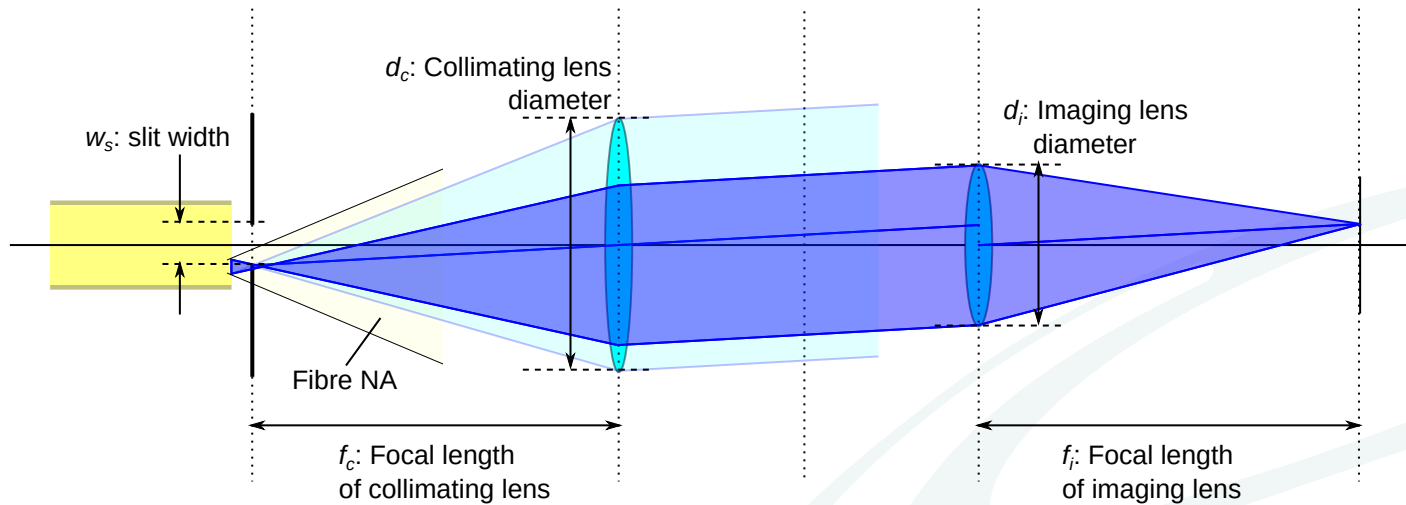
Instrument function width:  $w_i = M * w_s$

As wavelength range:  $\delta\lambda = \cos(\theta_a + \theta_g) \cdot w_s / (f_c k n)$

--> **Wavelength resolution set by slit width and collimating lens focal length**

# Throughput / Étendue

Throughput is determined by lens sizes and focal lengths:



Assuming  $NA > d_c / f_c$  and  $d_i / f_c$

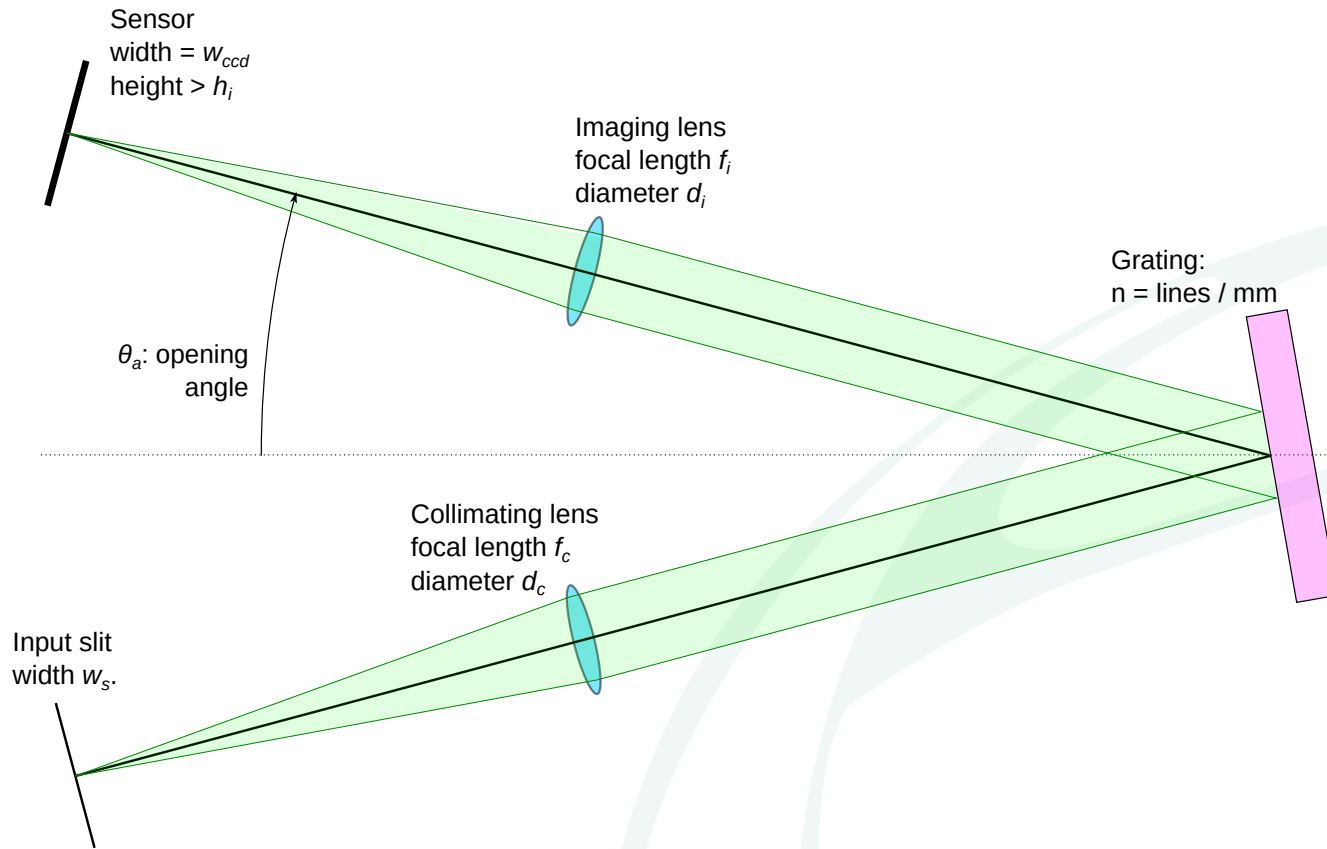
$$\text{Étendue} = d_f \cdot w_s \cdot \min(d_c, d_i)^2 / f_c$$

--> **Best signal with short focal length collimating lens and wide slit.**

Caveat: Diffraction grating efficiency usually reduces with higher n

# Configuration

Complete balance of configuration parameters:



Resolution:

$$\delta\lambda = A w_s / f_c$$

Range:

$$\Delta\lambda = A w_{ccd} / f_i$$

Throughput:

$$I = d_f \cdot w_s \cdot \min(d_c, d_i)^2 / f_c$$

Channels:

$$N_f = h_i f_c / f_i d_f$$

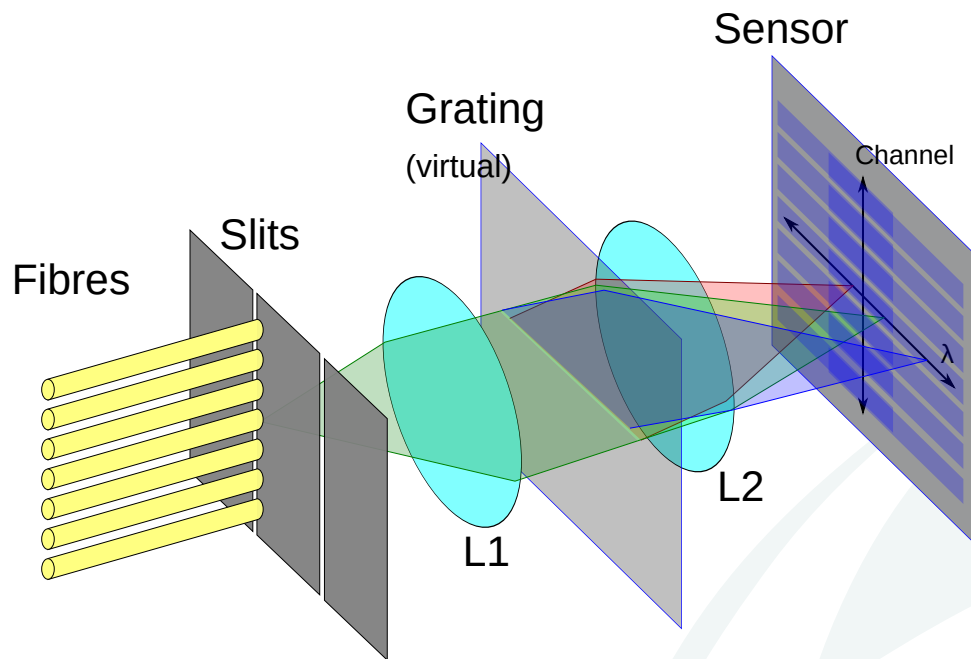
with  $A(\theta_a, k, n, l) = (1 - \frac{1}{4}k^2n^2\lambda^2)^{1/2} / kn - \theta_a \frac{1}{2} \lambda - \theta_a^2 / (kn (4 - k^2n^2\lambda^2)^{1/2})$

Change	Resolution	Throughput	Range	Channels	Economy
Sensor ↑	—	—	↑	↑	↓
Lens Size ↑	—	↑	—	—	↓
$f_i \downarrow$ (const $d_i$ )	—	—	↑	↑	↓
$f_c \downarrow$ (const $d_c$ )	↓	↑	—	↓	↓
Grating $n \uparrow$	↑	—	↓	—	—
Slit width ↑	↓	↑	—	—	—

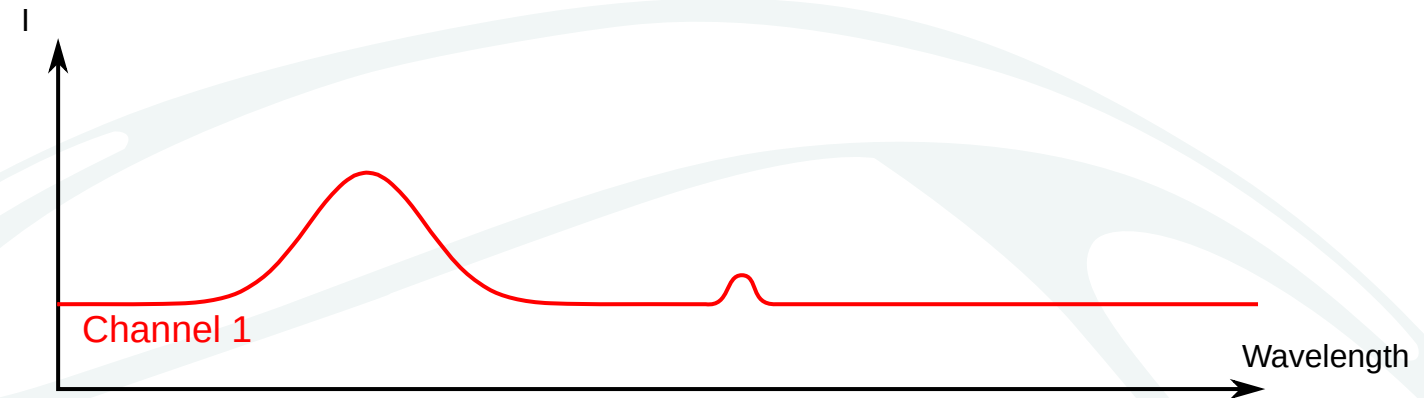
Gratings also have an efficiency that depends on wavelength, line density (n) and type.

# Other Configurations

It is possible to add extra channels, overlapping in the wavelength direction:

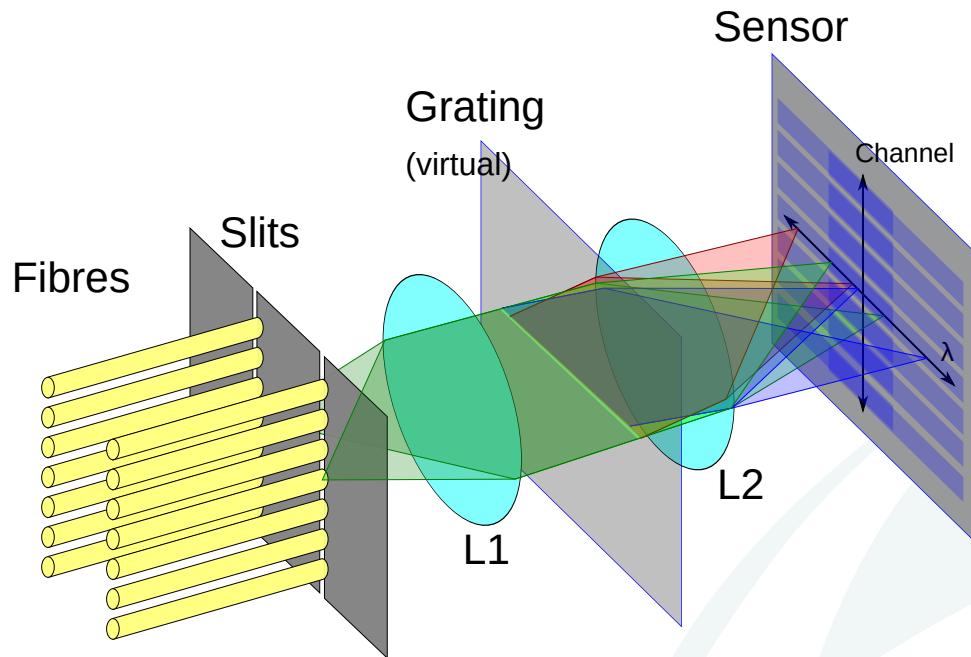


This only works if the vicinity of the target line is free from other lines. The spectra of overlapping channels add up, giving 2x background and hence higher noise:

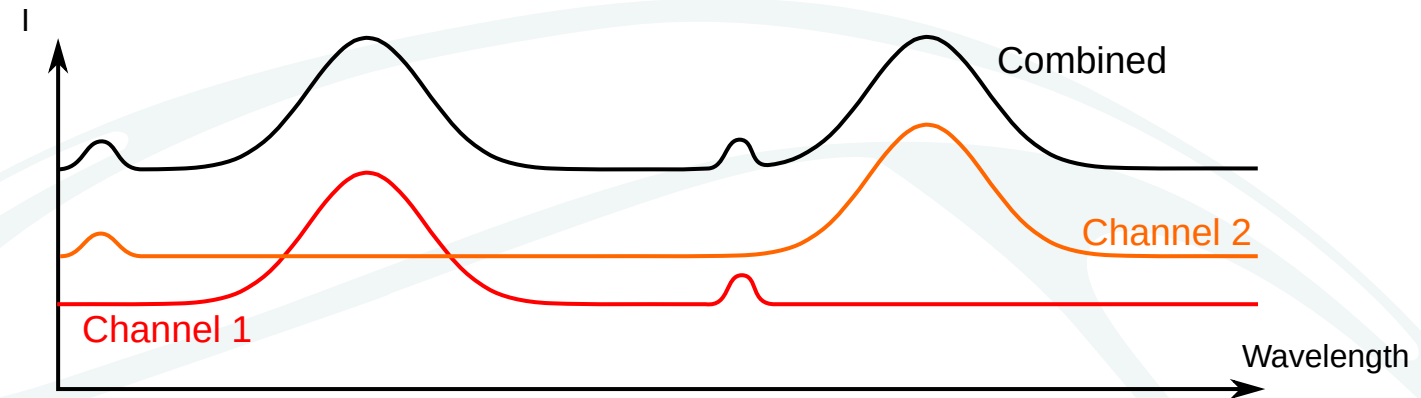


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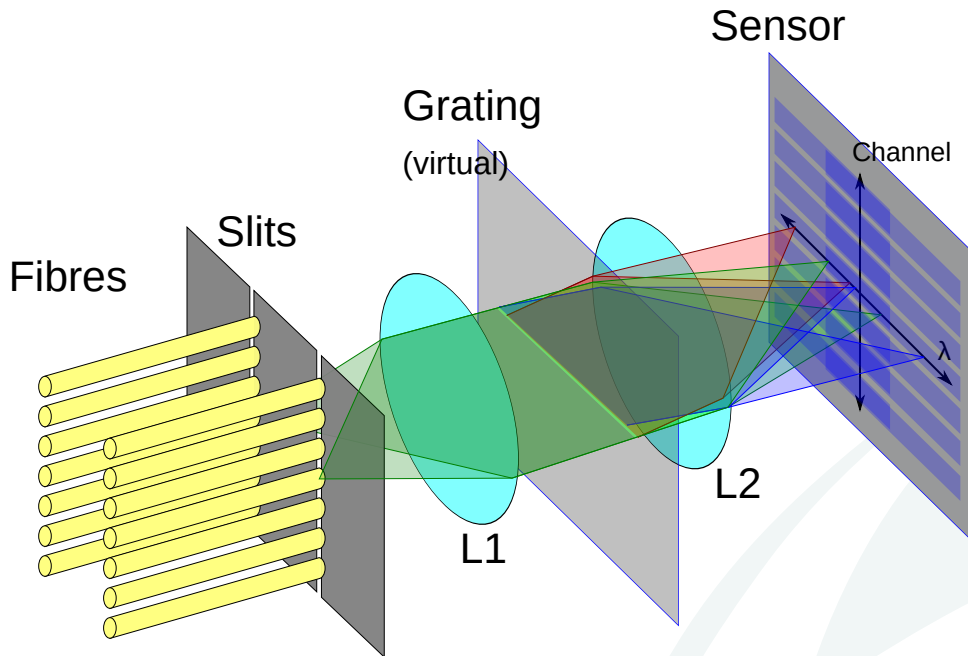


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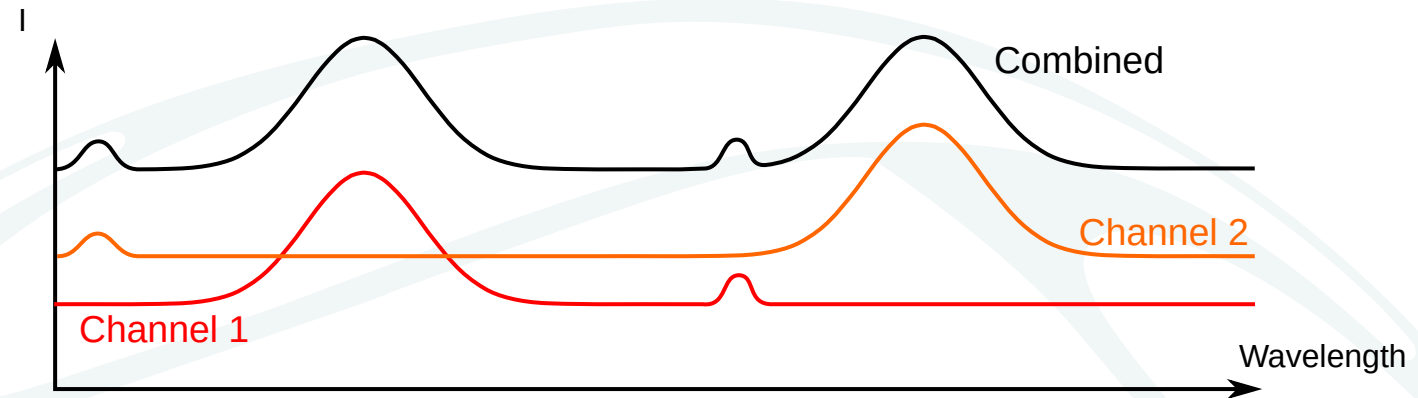


# Other Configurations

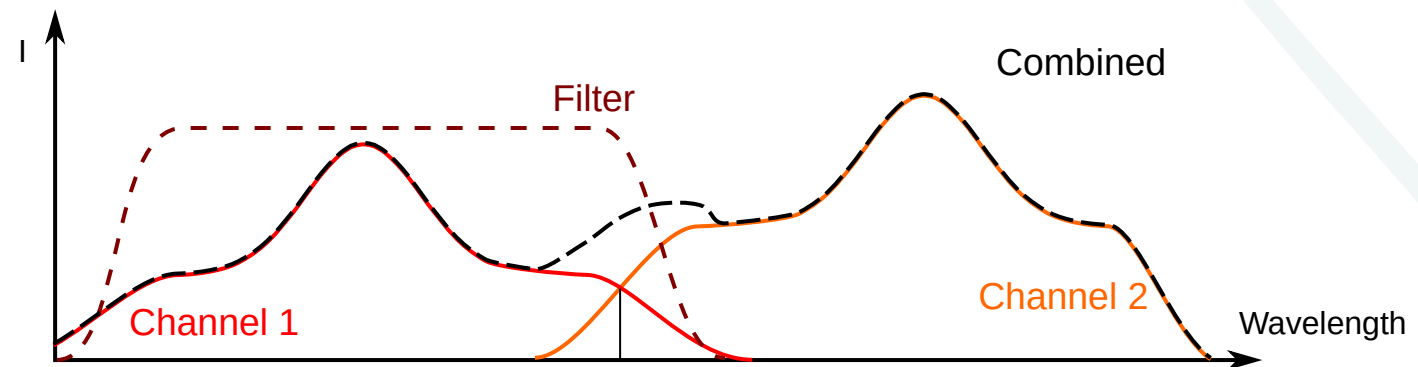
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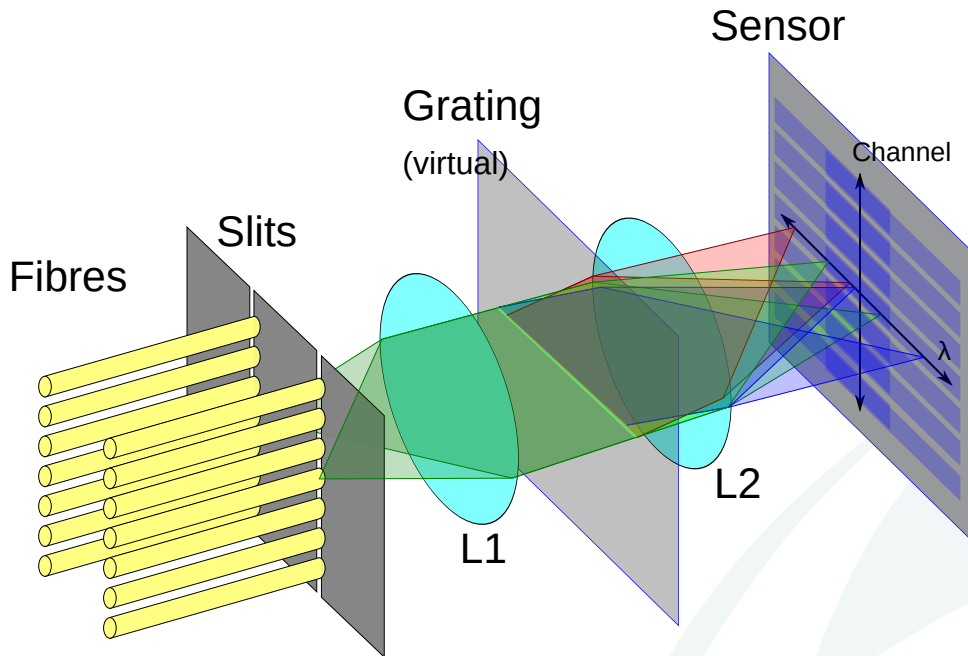


If too much contamination or noise is present, a bandpass filter can be added:

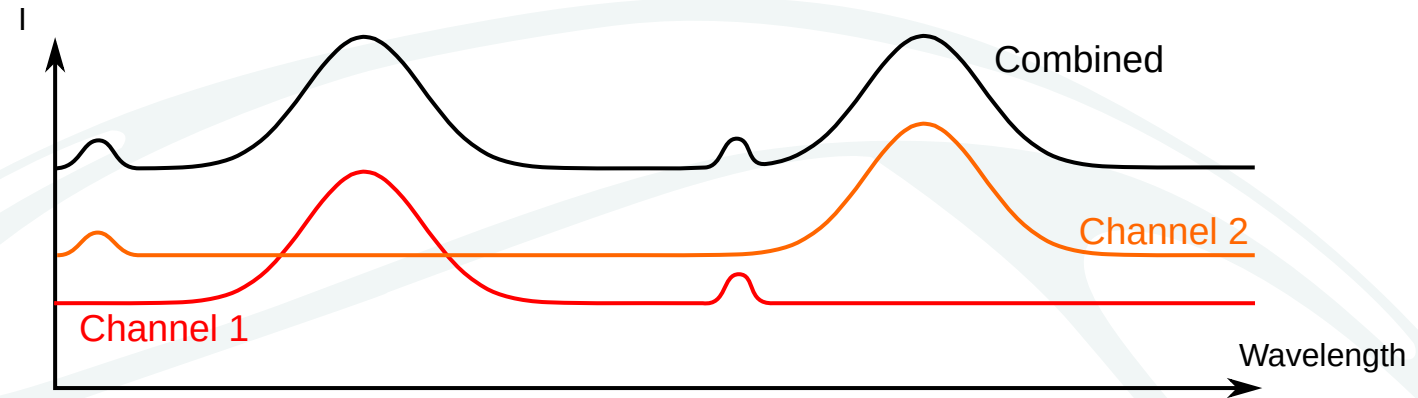


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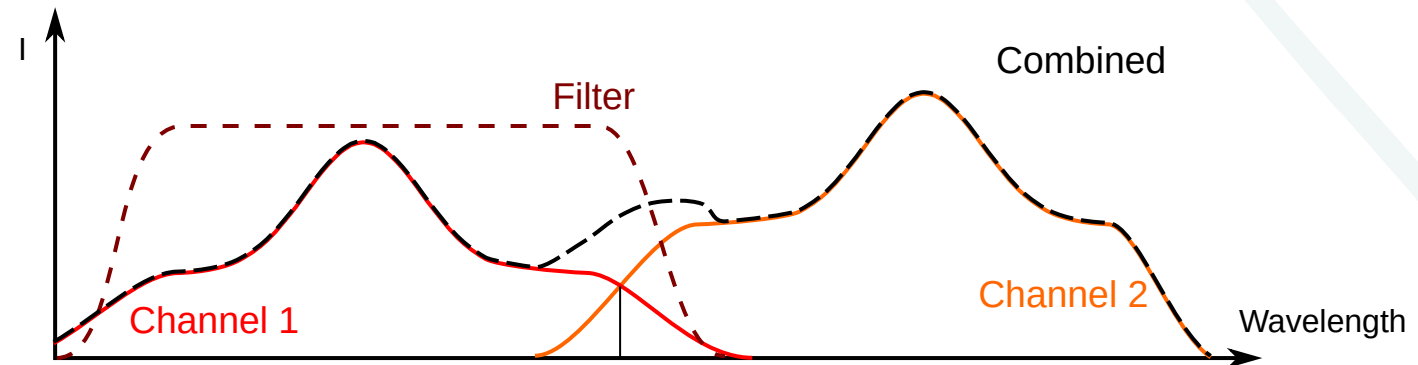
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If too much contamination or noise is present, a bandpass filter can be added:



## Full vertical binning:

If each column is filled with fibres from the same spatial channel and a CCD camera is used, the whole image can be binned into one row for very fast readout with a high signal level but a limited number of channels.

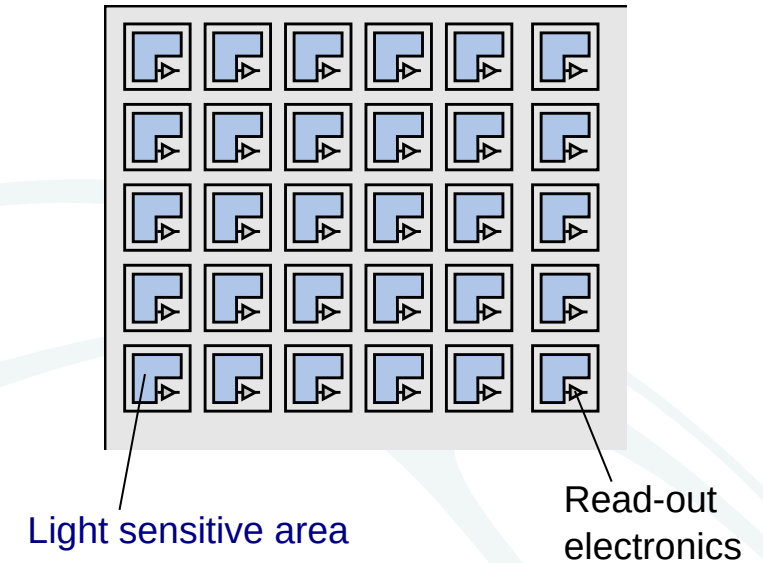


# Sensors: CCD vs CMOS

Two types of sensor are typically used:

CMOS: *Each pixel has its own read-out electronics.*

- Signal/noise is fixed per pixel and is not improved by binning.
- Frame rate can usually be increased by reducing vertical read-out range.
- Since each pixel has full bit-range (e.g. 16-bit), dynamic range is very high.



# Sensors: CCD vs CMOS

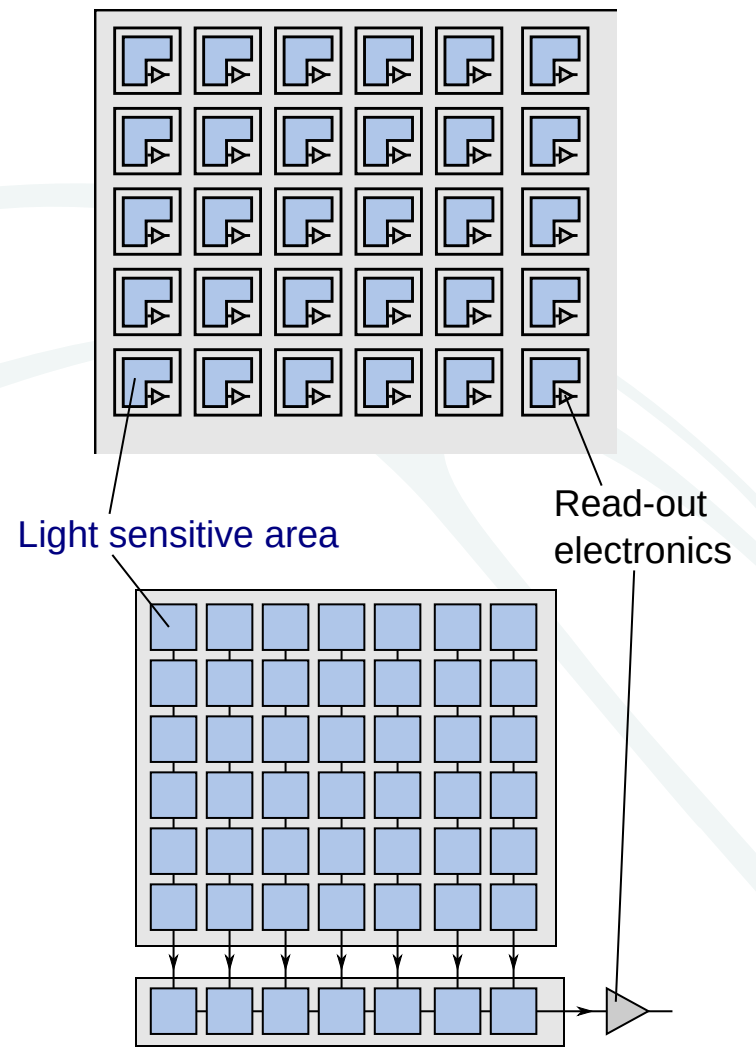
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- Signal/noise is fixed per pixel and is not improved by binning.
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- Since each pixel has full bit-range (e.g. 16-bit), dynamic range is very high.

CCD: Photoelectrons are moved down sensor and read-out sequentially.

- Signal/noise dramatically improved by binning pixels on the chip.
- Frame rate improved by binning or by less read-out area in any direction.
- Dynamic range limited by read-out row.
- Vertical smearing can be a problem if exposure time is very low.



# Set-up



Some spectrometers have few adjustments --> Less flexible but relies on machining accuracy but easier to set up.

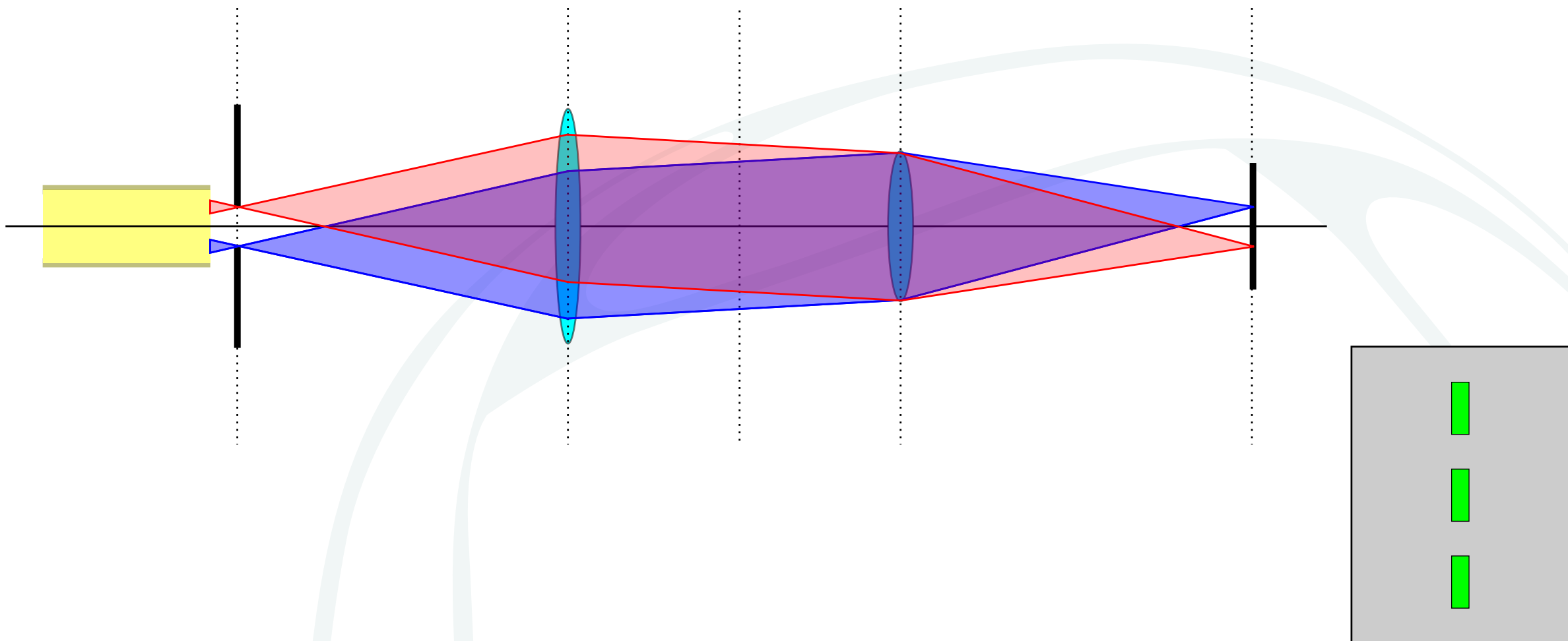
'Home-made' spectrometers or with more adjustments are very difficult to set-up initially.

Rough method (images and explanation on later slides): *\*TODO: We will test and adjust this procedure\**

- 1) Set both lens focuses close to infinity by imaging a far distant wall/building. If already in spectrometer, use a mirror or the grating.
- 2) Set all optical element heights and positions roughly as designing using linear-laser.
- 3) Set grating as mirror ( $\theta_g = 0$ ) and as close as possible to vertical using linear-laser back-reflection.
- 4) Set fibres as close as possible to back of slit. Open slit > fibres.
- 5) Light central fibre with a laser of known wavelength (e.g. HeNe @633nm), find grating angle motor position of that ( $\theta_g$ ).
- 6) Light all fibres with white light + neon lamp. Adjust brightnesses so stip and points are visible.
- 7) Set  $\theta_g=0$ , adjust CCD to centralise image.
- 8) Switch between  $\theta_g(\lambda \sim 500)$  and  $\theta_g=0$  and adjust grating lean until channel locations don't drift.
- 9) Adjust CCD tilt and grating tilt so that broadband lines are parallel to x on sensor.
- 10) Adjust both focuses to get sharp points in wavelength **and** channel directions.
- 11) Adjust fibre tilt to get channel column (or curve) symmetric.
- 12) Iterate 8-11 until no more improvement or satisfied with quality.
- 13) Close slit to  $\sim 1/2$  width of fibres. Adjust slit tilt and left/right position to match fibres.

# Focus

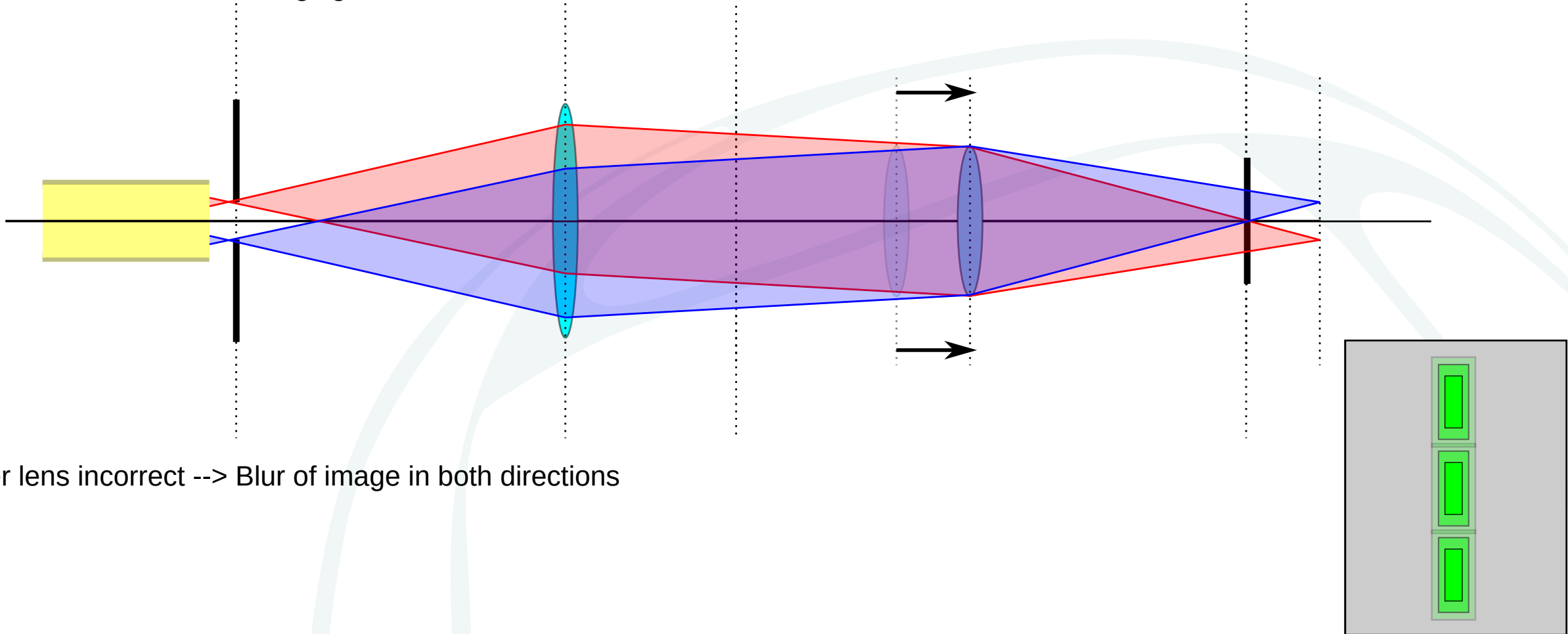
Both lenses have an optimal focus:



# Focus

Both lenses have an optimal focus:

Focus: Defocused imaging lens:

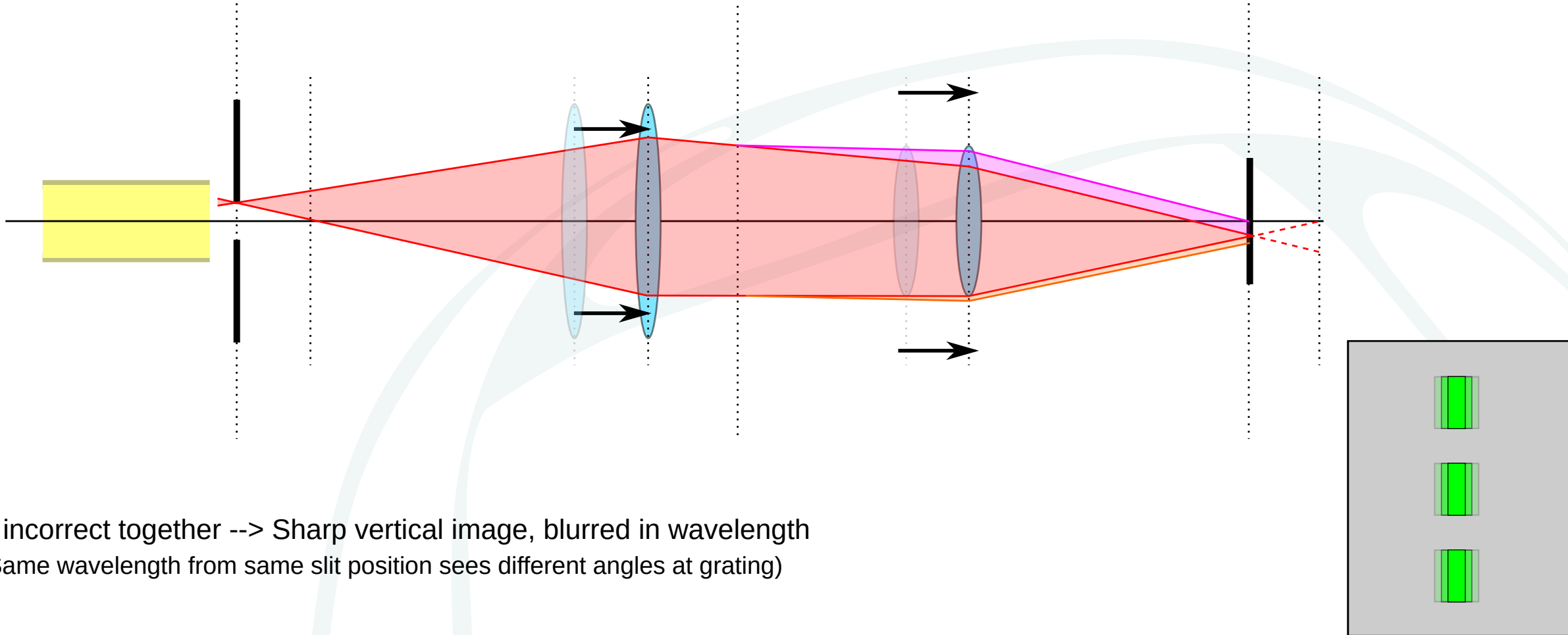


Either lens incorrect --> Blur of image in both directions

# Focus

Both lenses have an optimal focus:

**Focus: Compensated defocus of both lenses**



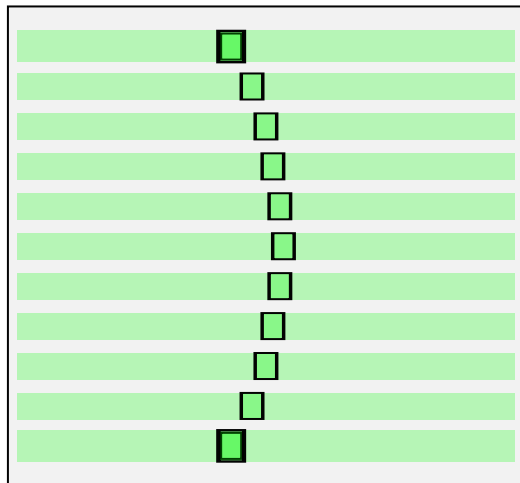
Both incorrect together --> Sharp vertical image, blurred in wavelength  
(Same wavelength from same slit position sees different angles at grating)

# Curvature

Due to second order effects, the diffraction changes slightly with vertical angle, causing a crescent shaped image of slit:

- 1) Light all channels with a narrow (Neon lamp) and wideband (white LED) source.
- 2) Scan the grating angle (wavelength setting)

Ideal alignment and focus should look like this:



Longest wavelength



Shortest wavelength

- Straight crescent shape (top and bottom displaced the same)
- Wideband lines are straight.
- Line drift minimal with wavelength setting change.
- All points focused as best as possible in both directions.  
(extreme top+bottom might be less well focused)
- Curvature might be more at longer wavelength

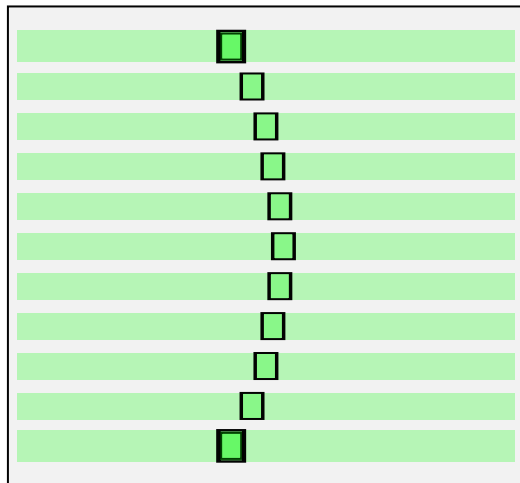


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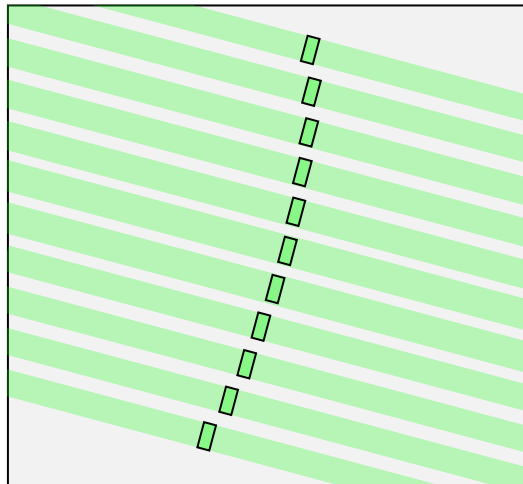


Shortest wavelength

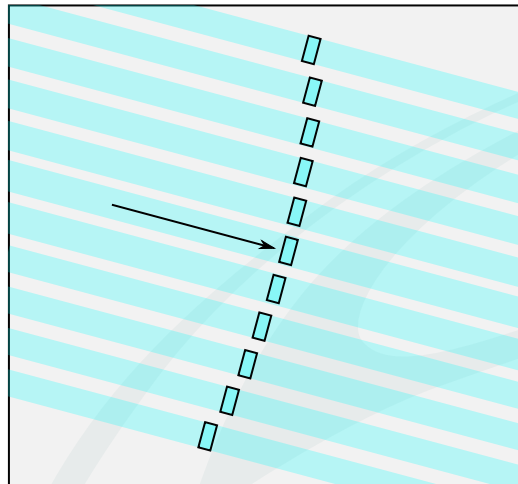
- Straight crescent shape (top and bottom displaced the same)
- Wideband lines are straight.
- Line drift minimal with wavelength setting change.
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(extreme top+bottom might be less well focused)
- Curvature might be more at longer wavelength

# Alignment

Mis-alignment of each component in any axis causes combinations of effects:



Longest wavelength



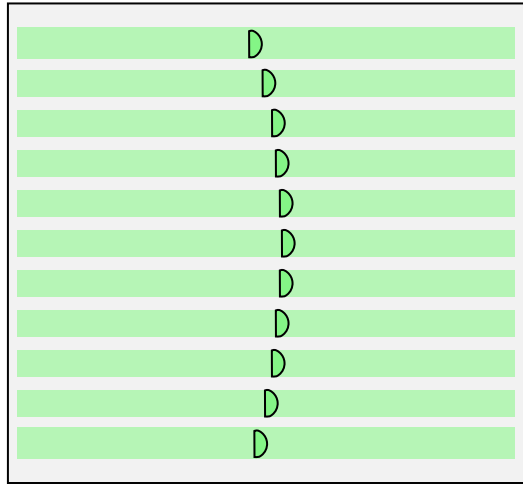
Shortest wavelength

Tilted sensor

Wideband lines and crescent are both tilted, but stay in place when wavelength setting (grating angle) is changed.

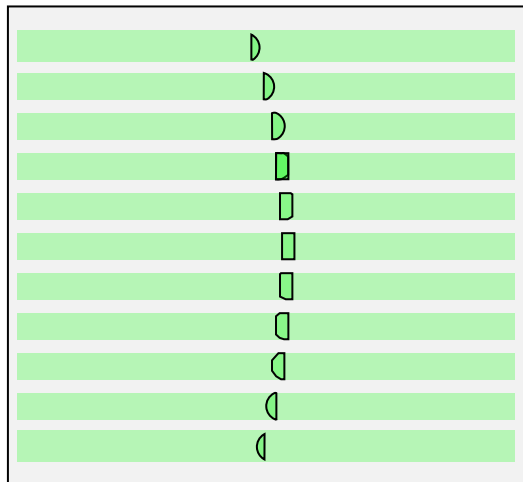
# Alignment

Mis-alignment of each component in any axis causes combinations of effects:



Shifted fibres relative to slit

- All fibres are out of slit in same direction

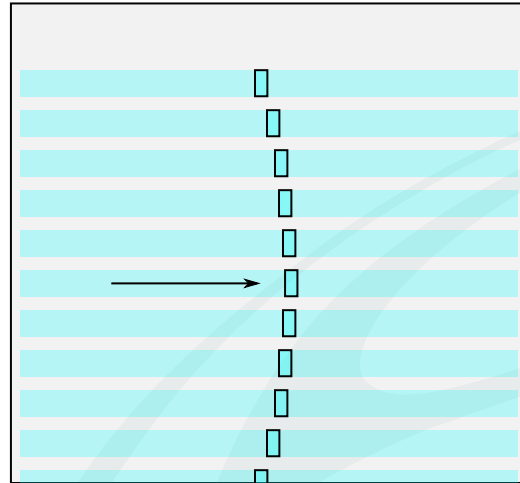
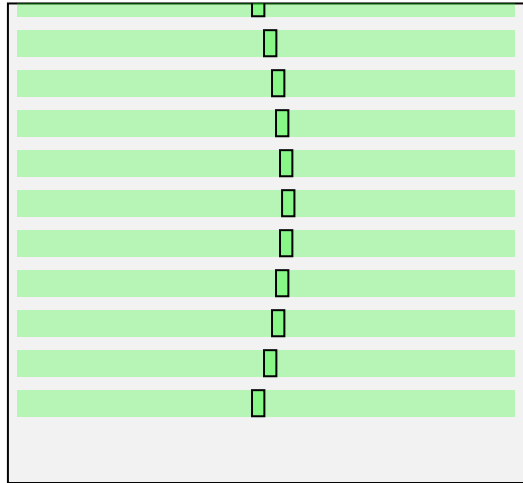


Tilted fibres

- Slit image is straight, but fibres move out of slit

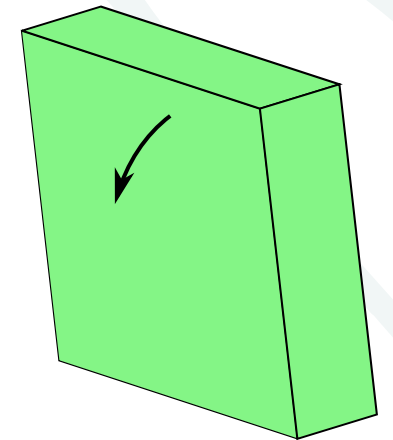
# Alignment

Mis-alignment of each component in any axis causes combinations of effects:



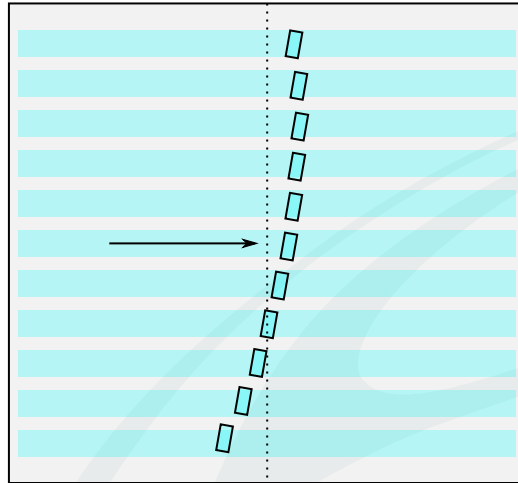
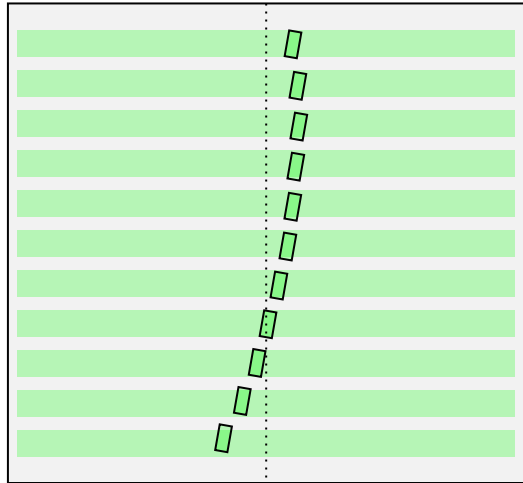
Tilted grating (forward)

- offset can be compensated at any wavelength by sensor or slit/fibre height, but will drift with wavelength (grating angle) change.



# Alignment

Mis-alignment of each component in any axis causes combinations of effects:

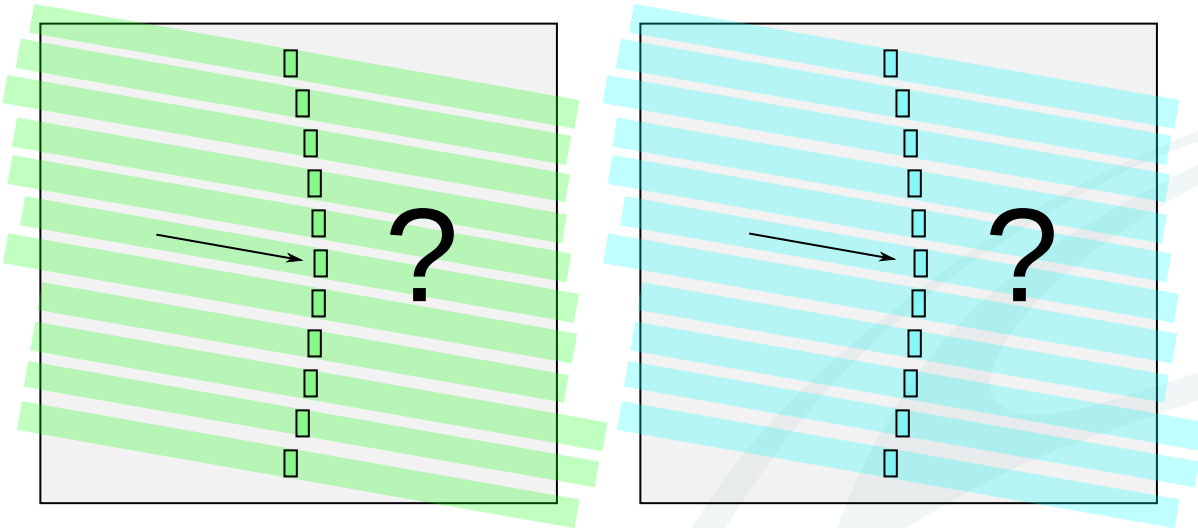


## Tilted Slit/Fibers

- Crescent angle tilted but wideband lines straight.
- Everything stays in position when wavelength changed

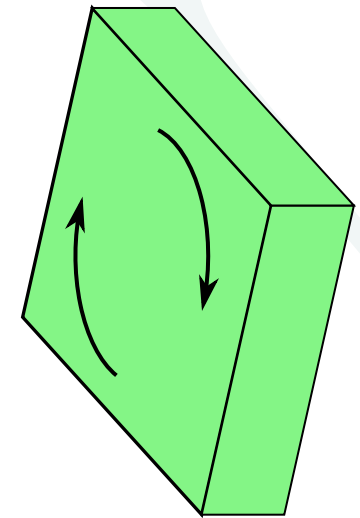
# Alignment

Mis-alignment of each component in any axis causes combinations of effects:



Tilted grating (in plane)

(I'm not entirely sure about this one yet).



# End



That's all folks

... at least for now ...