

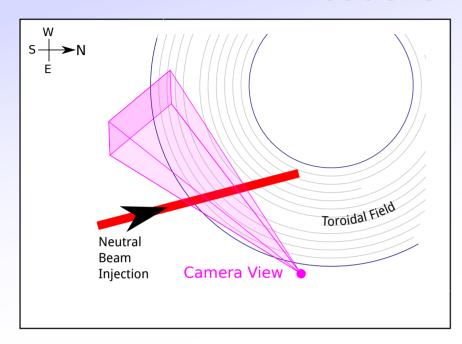


Motional Stark Effect Imaging: Development Progress and Initial Tests

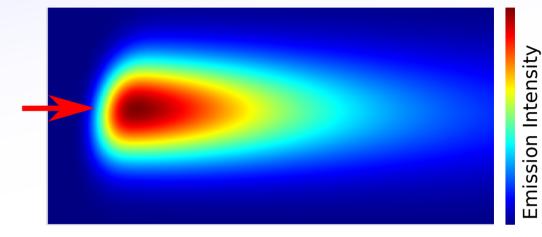
- O. P. Ford, J. Howard, R. Wolf 1
 - 1: Max-Planck Institut für Plasmaphysik, Greifswald, Germany
 - 2: Plasma Research Laboratory, Australian National University, Canberra
- Basic Principal
- Concept and Accuracy Tests
- Optics Design



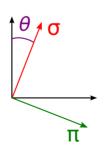
Introduction - Motional Stark Effect

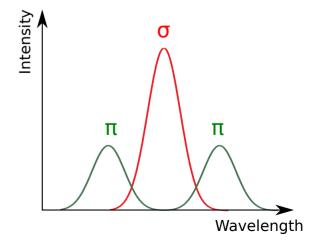


Neutral beam atoms injected into plasma. Excited by plasma, then emit $H\alpha/D\alpha$ radiation.



Polarisation of σ related to magnetic field direction, but π is always perpendicular with almost the same intensity so measuring the polarisation gives an unpolarised result if not spectrally separated.



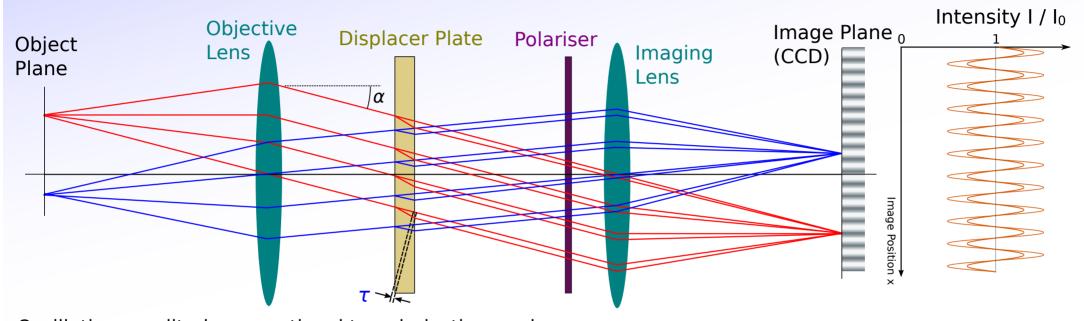






Inference Imaging with Displacer Plates

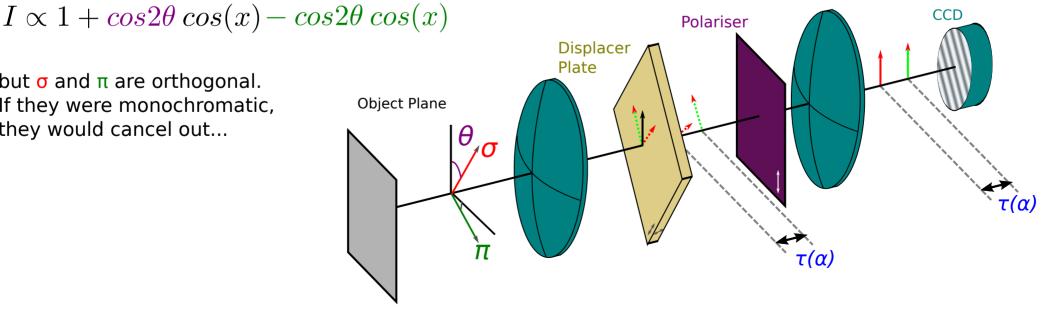
Displacer Plate: Angle dependent phase shift --> Interference pattern across image.



Oscillation amplitude proportional to polarisation angle.

but
$$\sigma$$
 and π are orthogonal. If they were monochromatic,

they would cancel out...





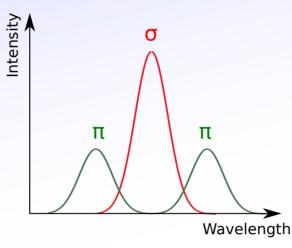


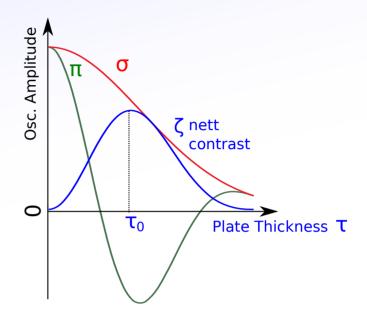
Spectral Coherence

Phase delay of a plate depends on wavelength. For large τ and finite spectral width, amplitude is reduced by decoherence.

For a specific τ , the phase of the π wings is 180° from σ. This cancels the 180° from the opposite polarisation, and the patterns add.

Add a delay plate to introduce the best τ_0 - where π and σ combine constructively.



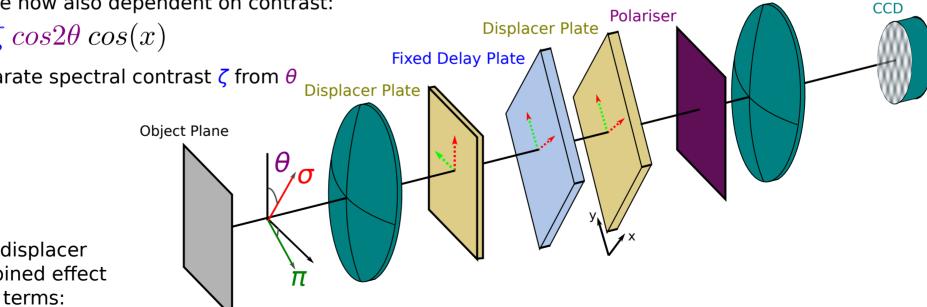


but amplitude now also dependent on contrast:

$$I \propto 1 + \zeta \cos 2\theta \cos(x)$$

Need to separate spectral contrast ζ from θ

add another displacer at 45°. Combined effect adds 2 extra terms:

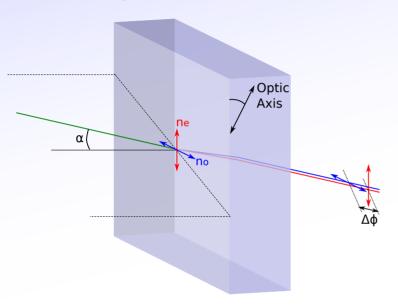


$$I \propto 1 + \zeta \cos 2\theta \cos(x) + \zeta \sin 2\theta \cos(x - y) - \zeta \sin 2\theta \cos(x + y)$$

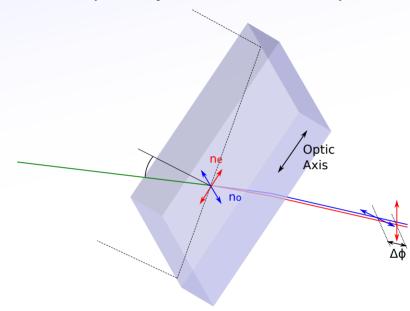


Concept Tests: Tilted Waveplates

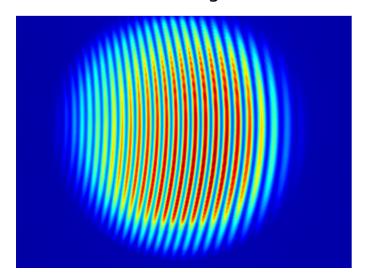
The displacer plates are uniaxial crystals cut at 45° to their optic axis:



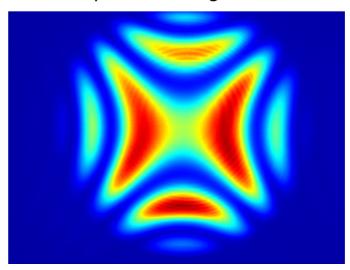
Before these arrive from Australia (today?), I have temporarily used tilted wave plates:



Delay pattern is a bit non-linear but, it still works well enough:



Incidentally, this happens a little with a flat waveplate and high field of view:



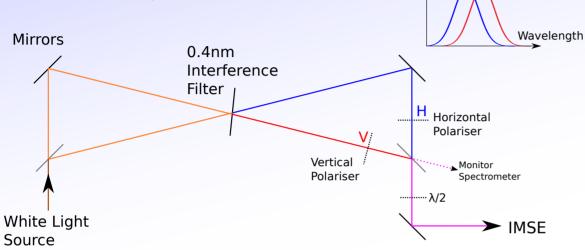




w/o delay w delay

Concept Tests: Simulated Spectrum

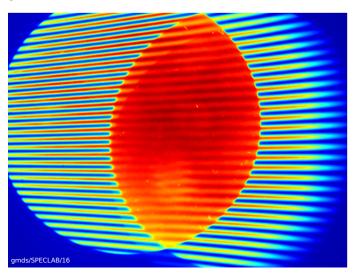
A way to simulate a known spectrum, with the same problem:

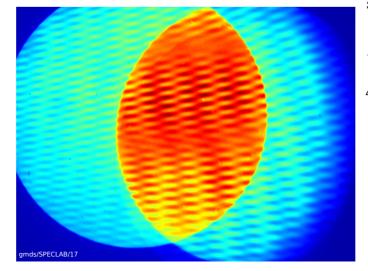


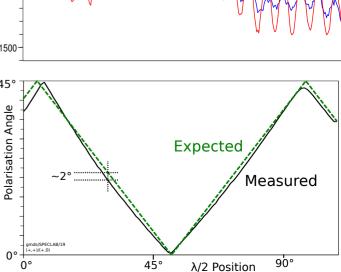
4880

With just one tilted plate and no net delay, separating the beams slightly we can see where the V and H polarisations cancel (well, almost):

Adding both displacer plates and a small net delay:



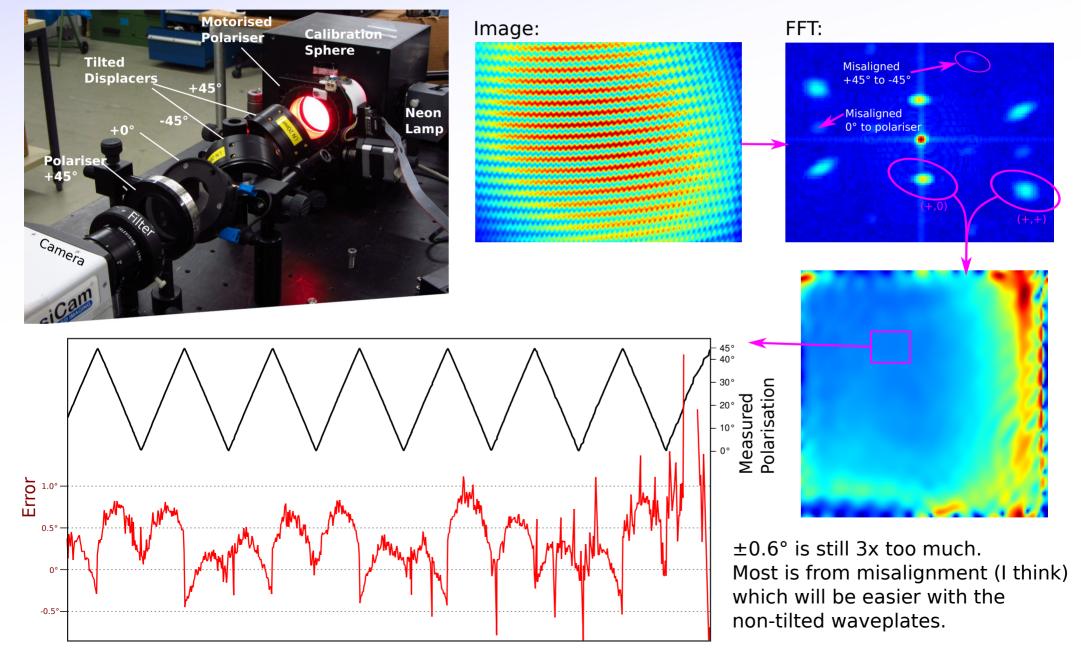




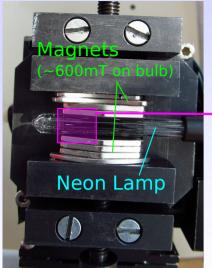


Concept Tests: Linear Polarisation

It worked as a concept test, but the accuracy was only $\pm 2^{\circ}$, possibly due to different V and H intensities. A slightly more accurate test, using single linear polarisaton:

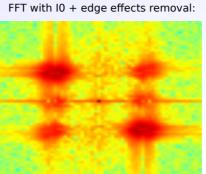


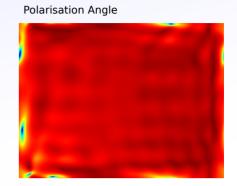




HDD Magnets Zeeman Lamp

Image (defocused)

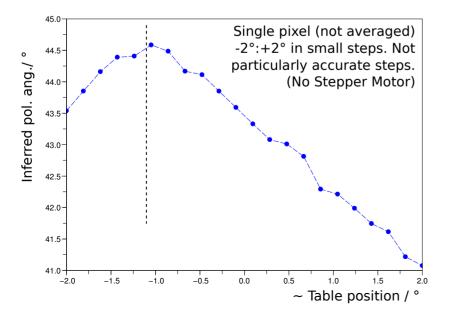


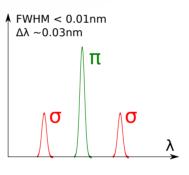


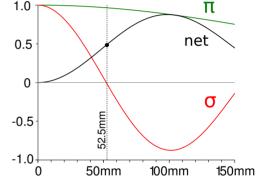
With 600 mT of hard disk magnets across the bulb, the 720 nm neon line is Zeeman split by about $\pm 0.03 \text{nm}$. As with MSE, light is net unpolarised so

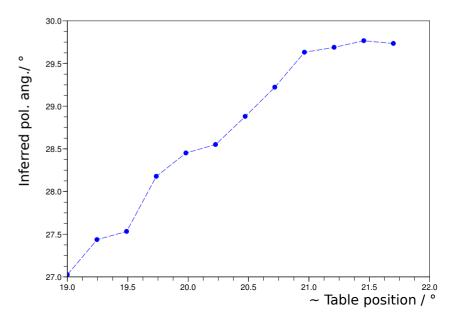
we need to exploit the coherence.

All the plates I have (~53mm of LiNb) is enough to cancel the o components (coincidentally).













IMSE Optics Design

The AUG IMSE system will couple to the existing MSE optics:

The design requires knowing the image that the existing optics will give, and how to optimally couple to it.

Developed a 3D ray tracer:

- Arbitrary multi-path ray trees.
- Models of basic camera lenses (Canon, Nikon, Schneider).
- Aspheric surfaces.
- Optimisation of all properties
- Polarisation state tracking.
- PSF and Imaging characterisation.
- Incoherent and/or coherent polarisation addition.
- 3D VRML output for rays, objects and polarisations (display e.g. in Sergei's 'wendel' program)
- Birefringent media (incl. E/O ray path splitting)

The ray tracer says:

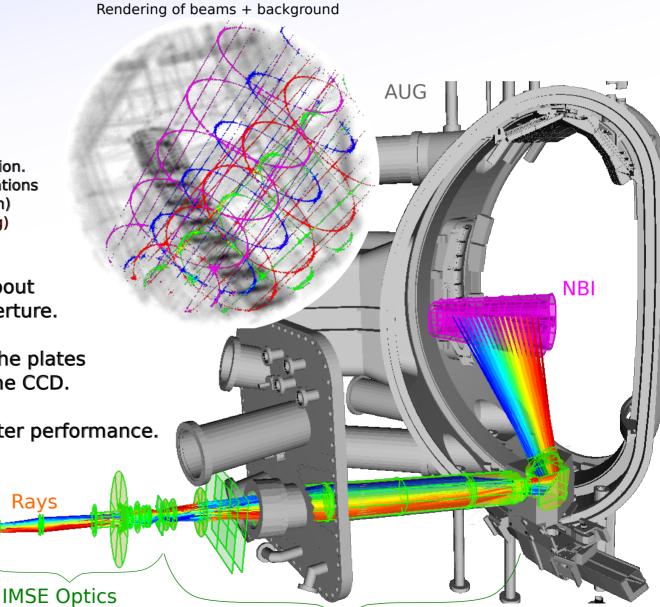
Delivery to back of MSE system is about 7% of total light hitting the first aperture.

For the first IMSE design (for which the plates were ordered) only 0.6% reaches the CCD.

More is possible, but it effects the filter performance.

Need to balance:

Throughput
Filter shift
Vignetting
Fringe frequency / linearity
Fringe imaging quality
Flexibility
Optics size/cost

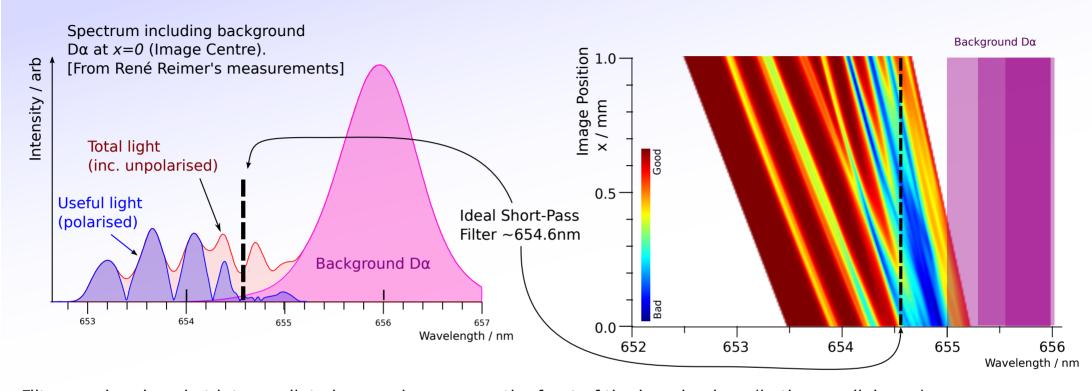


MSE Optics

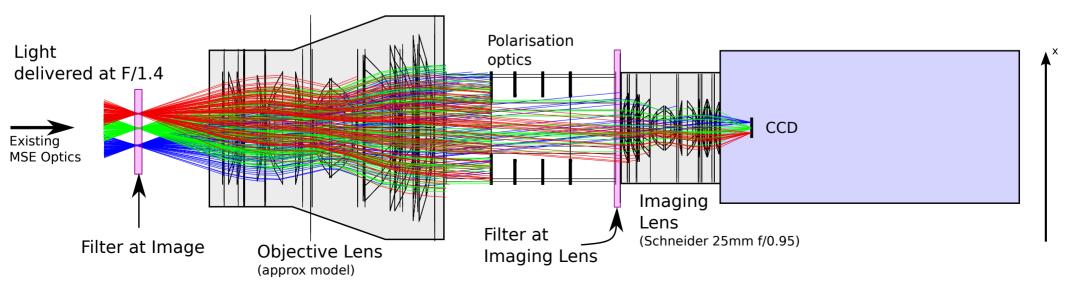


IMSE Design - Spectrum and Filter





Filter can be placed at intermediate image plane, or on the front of the imaging lens (in the parallel rays):





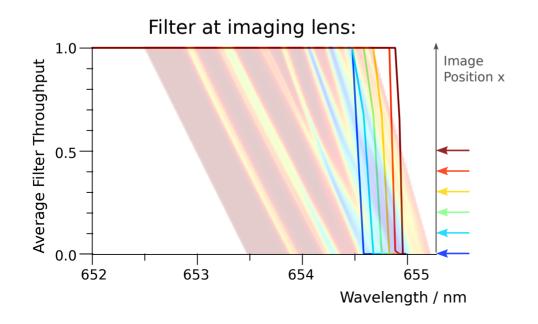
Oliver Ford, IPP Greifswald

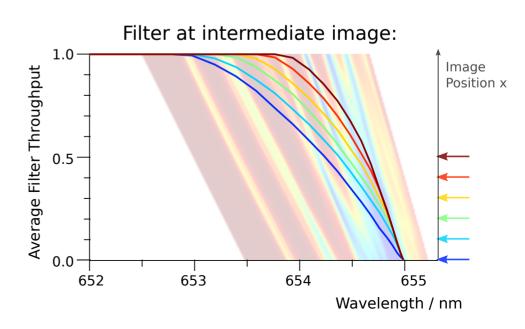
IMSE Design - Throughput and filter shift.

For the 'standard' case, light throughput is only ~ 0.6 % of MSE emission to mirror. Maximum possible is 7%.



Some proportion of the light goes through the filter at a very steep angle and shifts the filter short-pass into the useful spectrum. The filter functions for different image positions calculated by the ray tracer are shown below.









Oliver Ford IPP Greifswald

IMSE Design - Throughput and filter shift

Throughput of light, and angle of light through the filter depends on the pair of lenses. (It depends on the exact model of the lens, not just the focal length and F/#) 75mm: 25mm 105mm: 35mm 75mm: 25mm 180mm: 50mm 135mm: 50mm Fielded 2.0 -2.0 -(obj:img) 2.0% 1.2 1.0% Field lens improves vignetting for the 25mm ₹ 0.8 0.6% imaging lens. 0.4% 0.4 Filter at Image Plane: Inbetween field lenses: 0.5 Almost acceptable, but loses a lot of light. especially at edge. Filter at Imaging Lens: Significant improvement for the filter, and now with the possiblity of tuning it by tilting it. However, it requires a bigger filter. Almost all light is lost for edge. 654 653 75:25 gives ~3x more light than 135:50 but angles are too big for filter, and most/all light is lost at edge channel. In reality vignetting was also higher and edge of image is entirely lost (can only see ~19mm of fibre plane) Fielding the light after the cell into the imaging lens (should) solve the vignetting and It also helps with the filter a lot: Abs. worst case is Outside Edge --> ~200mm Collector Lens (perhaps as cell window) or 2x400mm to reduce abberations. Filter (75:25 Filter Fielded) (75:25 Unfielded) **Background** ~2x220mm Field Lenses 0.5 Filter between (shouldn't effect abberations) Imaging Lens For the fielded case at the very edge, it integrates up to about 66% of the good light under the filter which is 66% * 1.6% = 1% of **Good Light**

652

653

654

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But... abberation after plates hurts our fringe contrast so the collector lens needs to be good (without being a camera objective lens)

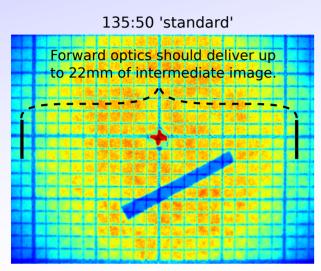
collected light, this is already > 2x the safe 135:50 case, and we're still at $\sim 3x$ for the rest image.

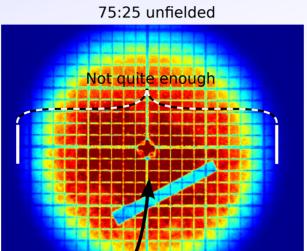


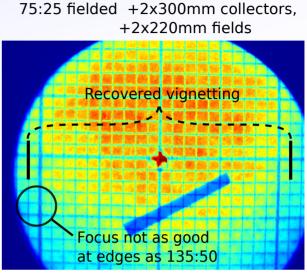
IMSE Design - Throughput and vignetting (lab test)

Oliver Ford IPP Greifswald

In the lab, the situation is similar, but a bit worse:



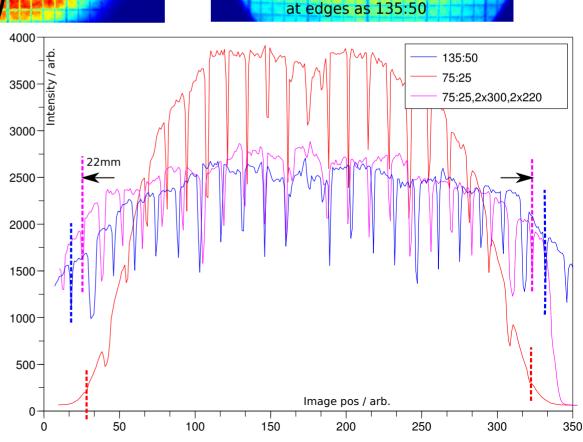




75:25 gives only a 50% increase in light in centre (1.5x as much as the 135:50) but the vignetting loses too much of the edge. The graph paper is at first image plane and we probably need to see 22mm of it.

Fielding fixes vignetting for 75:25 but uses 4 lenses. They are uncoated old lenses that were sitting in a cupbaord since 1960. All 4 lenses together only transmit $\sim 60\%$ of original intensity (measured) and leaves light level almost exactly back where we started.

However, with coated optimised lenses coupled with the improvement in the filter angles, it will improve the S/N by at least 50%.



IMSE Development Status Greifswald August 2012



IMSE Design - Status

Oliver Ford IPP Greifswald

2011

2012

- ✓ Modelling of AUG MSE emission spectrum/polarisation.
- ✓ Modelling of generated images and ability to infer polarisation angle images.
- ✓ Asses ability to infer axisymmetric current from polarisation images.
- ✓ Ray tracing of existing MSE optics to see the image delivered.
- Asses lens options for optics coupling.
- ✓ Calculate and order required crystals (for middle range of lenses)
- Calculate and order filter (approximate done, ••• order the optimal one)
- ✓ Investigate non-orthogonal fringes idea (works great)
- ~ ✓ Build polarisation test setup (simulated spectrum, OK, getting better filters).
 - ✓ Measurement principal test (Zeeman splitting).
- ~ ✓ Assess realistic polarisation accuracy.
- Develop experiment software (Camera, ADC, spectrometer, Calib. Stepper etc.)
- ✓ Software/Methods for exact alignment of plates.
- ✓ Assess neutron damage probability to camera (not much info, but looks OK)
- Design support structure.

Next...

- · Test camera under magnetic field.
- ••• Model polarisation effects of MSE forward optics.
- · · · Spectrum+Image model for MAST.
- ··· Calculate expected absolute light level (hence max absolute frame rate).
- ••• Find optimum optical setup (fielding etc).
- ··· Interface to objective auto-focus .
- ··· Lighting of background polarisers for absolute calibration.
- ••• Plasma-based absolute calibration method/check.
- ··· Add Stark/Zeeman coupling to forward model (Ellipticity).
- ••• Reproduce non-linearity in ray tracer (requires full E/O ray splitting to work)
- ••• Improve edge effect / non-periodic FFT demodulation problems.
- · Get support structure built.
- · · · Collect some data at AUG!

Much later...

- ✓ Modelling and image generation for W7X.
- ✓ Ability to infer polarisation angle for W7X images.
- ✓ Ability to infer parallel current for W7X.
- ••• W7X assessment based on AUG results.